file ACT/007/007 #6

0027

KAISER COAL

KAISER COAL CORPORATION
Sunnyside Coal Mines
P.O. Box 10
Sunnyside, Utah 84539
Telephone (801) 888-4421

August 23, 1988

RECEIVED
[redacted]
DIVISION OF OIL
GAS & MINING
PRICE, UTAH

Mr. John Whitehead
Utah Division of Oil Gas and Mining
355 West North Temple
3 Triad Center, Suite 350
Salt Lake City, Utah 84180-1203

Re: Sunnyside Subsidence Survey Data
Partial NOV Abatement
Permit No. ACT/007/007

Dear Mr. Whitehead:

Kaiser Coal Corporation submits the following subsidence data as a partial abatement of NOV 88-19-2-1:

1. Bear Canyon subsidence net control - 1986
2. Bear Canyon to Whitmore Dam level survey - 1986
3. Bear Canyon subsidence net control - 1987
4. Bear Canyon subsidence net control five additional stations - 1988

Kaiser Coal Corporation requests that the Failure to Abate Cessation Order be terminated upon receipt of this data. This submittal demonstrates Kaiser's good faith effort to abate the NOV by September 16th as previously requested. This effort is viewed as extraordinary response in light of the salary work force reduction to one from forty-eight during July.

Please let me know if this request is acceptable to the Division. Thank you for consideration in this matter.

Sincerely,

William P Balaz Jr

William P. Balaz, Jr. P.E.
Manager, Administration

6-7-88
B.F.A. 90.
DE. DL.

WARM WINDGUSTS

RADIAL SURVEY
TO LOCATE 5 ADDITIONAL
SUBSIDENCE MONUMENTS
IN BEAR CANYON

	B.S	T	F.S	T-19°C B2L.8" RPM 77
	ROMEO	OSCAR	S-010	
1	0° ~~0°~~	08° ~~04'~~	36.2 ~~23.7"~~	
2	38°	46'	12.2"	
1	218°	46'	29.4	
2	180°	08'	41.6"	
S			11.8 ✓	
@	38	37	41.9	
ADJ ∡	38	37	42.8	
	S-010	OSCAR	ROMEO	
1	0°	08'	52.3"	
2	321'	31'	03.5"	
1	141°	31'	17.7"	
A 2	180°	08'	56.1"	
BS S			10.4 ✓	
@	321	22	16.4 ✓	
ADJ	321	22	17.2	
360°			-01.7 ✓	

	OSCAR	TO	S-010	HI.	HS.
ZD	93°	10'	57.3"	4.75'	5.26
ZR	266°	49'	04.7"		
S			02.0 ✓		
@	93	10	56.3 ✓		
Z∡MN.	93	10	16.6		
S.DIST.	8,184.715		HED=	8,172.181	
RETURN SIGNAL-07			GRID=	8,172.345	

	S-010	TO	OSCAR	
Z D	86°	50'	25.0"	
R	273	09	38.7	
S			03.7	N 66,347.74
@	86	50	23.2	E 53,540.573
S-010 EL.	7444.395			

T
B
PRM

ROMEO - OSCAR - S-09

1	0°	03'	51.4
2	31°	24'	32.0
1	217°	24'	41.2
2	180°	04'	06.2
S			5.6 ✓
@	37-20-37.8		
ADJ	37-20-41.1		

	S-09	OSCAR	ROMEO
1	0°	25'	52.8"
2	323	05	11.1"
1	143	05	20.8'
A 2	180	26	08.3
BS S			5.8 ✓
BS @	322-39-15.4		
BADJ	322-39-18.9		
360			-06.8

	OSCAR	TO	S-010	HI	HS
ZD	93	46	01.7	4.75	5.21
ZR	266	14	02.7		
S			04.4 ✓		

@ 93-45-59.5
M 93-45-25.0
S DIST 7,629.085 HED.= 7,612.690
RTN. SIG.-06 GRID= 7,612.859

S-09 TO OSCAR

ZD	86-15-08.1	N 66,008.66
R	273-44-49.1	E 53,061.73
S	02.8	
@	86-15-09.5	
S-09 EL = 7397.162		

	BS	π	FS	T B PRM
	BOMEO	OSCAR	S-08	
1	0°	04'	20.4"	
2	36°	17'	23.9"	
1	216°	17'	38.8'	
A 2	180	04'	32.8	
S			2.5 ✓	
BS @	36	13	04.9	
ADJ 4	36	13	02.8	
	S-08	OSCAR	BOMEO	
1	0	04	16.3	
2	323	51	14.1	
1	143	51	26.6	
2	180	04	29.2	
A S			0.4 ✓	
BS @	323	46	57.6	
B ADJ	323	46	57.3	
360°	+2.4 ✓			

	OSCAR	TO	S-010	HI	H.S.
ZD	94	26	~~19.1~~ 16.0	4.75	5.28
ZR	265	33	53.4 ~~54.4~~		
C S			~~10.4~~ 09.4		
BS @	94	26	11.3		
M	94	25	39.0		

S DIST 6,966.65 45 HZD= 6,945.855

RTN. SIG. -10 GRID= 6,946.021

	S-08	TO	OSCAR	
Z D	85	34	50.0	
R	274	25	03	
S			07.0	N 65,552.95
@	85	34	53.3	E 52,554.32

S-08 EL= 7358.973

	BS	π	FS	T B PRM
	BOMEO	OSCAR	S-07	
1	0°	05'	56.3	
2	35°	34'	06.4	
1	215°	34'	19.1	
2	180°	06'	17.0	
S			8.0 ✓	
@	35-28-06.1			
ADJ	35-28-09.1			

	S-07	OSCAR	BOMEO
1	0	05'	57.4
2	324	37'	48.8
1	144	37'	57.6
2	180	06'	09.8
S			3.6 ✓

@ 324-31-49.6

ADJ 324-31-50.9

360° -4.3 ✓

	OSCAR	TO	S-010	HI	HS
ZD	95	02	13.6	4.75	5.24
ZR	264	57	51.3		
S			4.9 ✓		

@ 95-02-11.2

M - 95-01-36.8

S.DIST. 6386.413 HZD 6361.849

RTN. SIG. -11 GRID- 6,362.007

S-07 TO OSCAR

ZD	84-58-55	
R	275-01-00	N 65,124.49
S	05	E 52,148.08

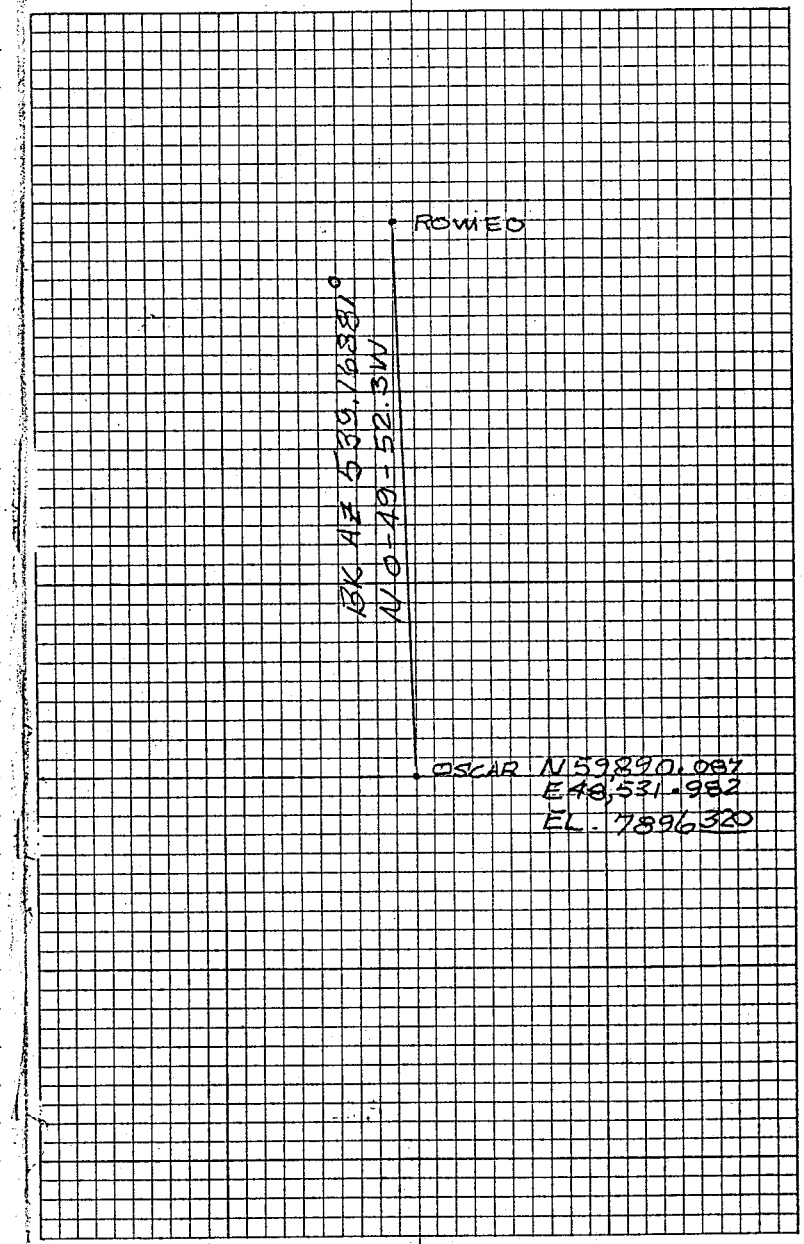
@ 84-58-57.5

S-07 EL = 7337.063

	BS	T	FS	TB PRM
	ROMEO	OSCAR	S-06	
1	0	05	16.5	
2	33	52	30.9	
1	213	52	38.4	
2	180	05	25.6 ✓	
Δ <			1.6	
@	33	47	13.6	
ΔR1	33	47	14.0	
	S-010	OSCAR	ROMEO	
1	0	05	10.7	
2	326	17	58.9	
1	146	18	05.6	
2	180	05	27.3	
Δ S			09.9 ✓	
@	326	12	43.3	
ΔADJ	326	12	46.1	
360°			-3.2 ✓	

	OSCAR	TO	S-006	HI	HS
ZD	96	04	42.3	475	541
ZD	263	55	23.2		
Δ S			5.5 ✓		
@	96	04	39.6		
M-	96	04	07.5		
ST-1	5795.135		HED = 5,762.658		
RTN. SIG. 09			GRID = 5,762.814		
			S-06 EL = 7283.670		

	S-06	TO	OSCAR	
Z D	83	56	24.2	
R	276	03	35.1	N 64,725.60
S			00.7	E 51,666.93
@	83	56	24.6	



1988 SUBSIDENCE MONITORING
BEAR CANYON NET 8/23/88

T- 22°C
B- 22.2"
PPM- 76

		OSCAR TO SUB			HI	HS
Z	D	100°	55'	29.9"	4.85'	
	R	259°	04'	33.8"		
	S			3.7"		
	@	100°	55'	28.1"		
2X ADJ.						
SD		3503.600'				
HZD						
EL						

T- 28°C
B- 22.8
PPM 74

OSCAR EL =

		S-1	TO	SUB	HI	HC
Z	D	78°	35'	41.8"	5.01'	
	R	281°	24'	30.9"		
	S			12.7"		
	@	78°	35'	35.5"		
2X ADJ.						
S.D.		350.260'				
HZD						

D.	78°	35'	46.9"	
R.	281°	24'	23.9"	
S.			10.8"	
@.	78°	35'	41.5"	

T-
B-
PPM-

	OSCAR TO SUB			HI	HS
Z D					
R					
S					
@					
2X ADJ					
SD					
HZD					
EL					

T-
B-
PPM-

OSCAR EL =

	S-2	TO	SUB	HI	HS
Z D	85°	33'	46.7"	5.99'	
R	274°	26'	21.8"		
S			8.5"		
@	85°	33'	42.4"		
2X ADJ					
S.D.	570.920'				
HZD					

10/10/87
BFA-KRH-DL.

№ 7 SHOOTING
OF
BEAR CANYON
SUBSIDENCE
NET

DBL VS

T2'S & AUTO BANKED

TEM — 64°
BARO — 21.8"
PPM — 109=1

T@ OSCAR FS. SUB.

ZD	100°54'54.7"				
DEP. R	259°05'12.6"				
S	7.3" ✓				
@	100°54'51.1" ✓		* AUG	100 54	39.2
ZD	79	05	31.2		
INCL. R	280	54	26.1		
S			02.7 ✓		
@	79	05	32.6	AUG 79	05 20.8
	OSCAR	TO	SUB	HI	HS
S. DIST	3503.31			1520MM	1389MM
				4 99	4 56

HZ DIST 3440.081

SUBEL 7233 88

OSCAR EL. 7896.32

10/7/86 7233 705

TEM — 68°
BARO — 22.6"
PPM — 103=0

	T	@	S1	F.S.	SUB.
ZD	78° 26' 13.9"				
R	281° 33' 43.9"				
DEP. S	2.2" ✓				
@	78° 26' 15.0"	* AUG	78 26	11.4	
ZD	101 33 55.1				
R	258 26 16.8				
INCL. S			05.9		
@	101 33 52.2	AUG	101 33	48.6	
	S1	TO	SUB	HI	HS
S. DIST.	350.32			1490MM	
				4 89	4 56
HZ DIST.	343.092				
S1 EL =	7163.329				

10/7/86 7163 176 S1

10/10/87 7163 329

UP 0.153'

TEM. – 70°
BARO – 22.6"
PPM – 104 =

	T @ S_2 F.S. SUB.			
ZD	~~85° 28' 06.2"~~ ~~85° 28' 05.8"~~			
R	~~274° 31' 42.9"~~ 274° 31' 45.2"			
DEP. S	8.6" ✓			
@	85° 28' 10.5" ✓ * AVG. 85-28-04			
ZD	94	32	04.2	
R	265	27	59.0	
INCL. S			03.2	
@	94	32	02.6 AVG. 94-31-56	
	S_2 To SUB.		HI	HS
S. DIST.	570.94'		1628 MM	
HZ. DIST.	569.156'		5 34	4 56
S_2 EL =	7187 991			
10/7/86	7188 053			
10/10/87	7187 991			
	DOWN 0.062'			

TEM. – 72°
BARO. – 22.5"
PPM. – 105 =

	T @ S_3 F.S. SUB.			
ZD	88	04	44.7	
DEP. R	271°	55'	11.0"	
S	4.3" ✓			
@	88°	04'	46.9" ✓	
	* AVG. 88 04 41.1			
ZD	91	55	25.2	
R	268	04	35.9	
INCL. S			01.1	
@	91	55	24.7 AVG. 91 55 18.9	
	S_3 To SUB.		HI	HS
SDIST	928.46'		1581 MM	
HZ. DIST =	927.939'		5 19	4 56
S_3 EL =	7202 130			
10/7/86	7202 583			
10/10/87	7202 130			
	DOWN 0.453'			

TEM. — 75°
BARO. — 22.6"
PPM — 105 =

T @ S4 F.S. SUB.

ZD	~~89° 30' 58.8"~~ ~~89° 30' 55.4"~~ ~~270° 28' 42.7"~~ 89° 30' 53.4"		
DEP. R	270° 28' 44.9"		
S	16.3"		
@	89° 31' 06.9"		
		*AVG.	89 31 04.2
ZD	90	29	01.2
INCL. R	269	31	04.1
S			05.3
@	90	28	58.6 AVG. 90-28-55.8

S4 TO SUB.	HI	HS
S. DIST. 1359.77'	1597MM	
HZ. DIST = 1359.723'	5 24	4 56
S4 EL = 7221 795		

10/7/86 7223 339
10/10/87 7221 795

DOWN 1.544' ?

TEM. — 75°
BARO. — 22.6"
PPM. — 105 =

T @ S5 F.S. SUB.

ZD	~~90° 32' 17.3"~~ 90° 32' 13.9"		
R	269° 27' 28.6"		
DEP. S	14.1"		
@	90° 32' 24.4"		
		*AVG.	90-32-16.7
ZD	89 27 53.8		
R	270 32 11.9		
INCL. S			05.7
@	89 27 50.9	AVG.	89 27 43.3

S5 TO SUB.	HI	HS
S. DIST. 1834.87	1523MM	
HZ DIST = 1834.758'	5 00	4 56
S5 EL = 7250 737		

10/7/86 7250 666
10/10/87 7250 731

IP 0.065'

TEM. – 74°
BARO. – 22.6"
PPM. – 105 =

	⊼ @	SUB	BCS2		
	ZD	~~91° 48' 35.8"~~ 91° 48' 42.6"			
DEP.	R	268° 11' 08.3"			
	S	9.1"			
	@	91° 48' 47.1"			
			* AVG.	91-48-39.1	
	ZD	88	11	29.1	
INCL.	R	271	48	31.5	
	S			00.6	
	@	88	11	28.8	AVG. 88-11-20.9

	BCS2	TO	SUB.	HI	HS
S DIST.	2949.72'			1471MM	
HZ. DIST.	2948.235			4.83	4.56
BCS2	7327.001				

OSCAR - SUB - BCS2

1	0	07	52.4
2	210	06	17.0
1	30	06	07.9
2	180	07	42.1
S			01.2
@	209	58	25.2
			ADJ. 209 58 25.7
1	0	06	21.2
2	150	07	43.9
1	330	07	53.1
2	180	06	21.5
S			08.9
@	150	01	27.2
			ADJ. 150 01 30.7
360			-04.0

VOID POINT NOT USED

10/7/86
B. F. A
M. OLSON

6TH SHOOTING
BEAR CANYON
SUBSIDENCE NET

DBL. V4's

T-2's
TOPCON

	OSCAR	TO	SUB
ZD	100	54	25.3 29.6 +0.7
R	259	05	31.4 5
S			01.1 ✓
@	100	54	29.1 ✓
Z*M	100	54	15.2
SD.	3503.	235	

TEMP = 56°
BARO = 22.1"
PPM = 71

	HI	HS
	1390 mm	1368 mm
	4560'	4488'

	SUB	TO	OSCAR
ZD	79	05	53.8
R	280	53	56.0
S			10.5 ✓
@	79	05	58.7 ✓
Z&M =	79	05	44.8
HZD	3440.	040	
DAT. EL	7233	705	

OSCAR - SUB - S-1

1	0	07	15.4
2	271	53	22.2
1	91	53	31.8
2	180	00	12.4
S			7.6 ✓
@	271	53	15.6 ✓
ADJ.	271	53	13.0
1		01	17.3
2	88	08	14.4
1	268	08	15.3
2	180	01	30.1
S			11.9 ✓
@	88	06	51.1 ✓
ADJ.	88	06	47.0

360° + 6.8" ✓

	SUB	70	S1
ZD	101	29	40.5
ZR	258	30	17.2
S			02.3 ✓
@	101	29	41.7 ✓
SD	350.405		
Z&M =	78	30	18.2
Z&M =	101	29	41.8

TEMP 62°
BARO 22.5"
PPM 70

HI	HS
1351 mm	1565 mm
4432'	5134'

HZD = 343.378
DAT. EL 7163 176

	OSCAR	SUB	S-2			
			56.7			
1	00	04	00			
			51.5			
2	227	08	58.8			
1	47	09	04.0			
2	180	03	54.4			
S			12.7	✓		
@	227	05	01.2	✓		
ADJ	227	05	01.4			
1		03	11.1			
2	132	58	15.4			
1	312	58	14.3			
2	180	03	21.9			
S			11.9	✓		
@	132	54	58.4	✓		
ADJ	132	54	58.6			
360°			-0.5	✓		
	SUB	TO	S-1	HI	HS	
ZD	95	25	52.6	1351mm	1815mm	
R	265	34	00.6	4432'	5955'	
S			06.8	✓		
@	94	25	56.0	✓		
SD	570.985					
Z*M	85	34	00.2	2nd	99 25	59.8
HZD	569.278					
DAT. EL	7188	053				

OSCAR - SUB - S-3

1	0	08	46.3
2	218	45	35.6
1	38	45	45.1
2	180	08	47.7
S			08.2 ✓
@	218	36	53.3 ✓
ADJ	218	36	55.5
1	0	05	24.6
2	141	28	30.1
1	321	28	28.9
2	180	05	27.9
S			04.5 ✓
@	141	23	03.3 ✓
ADJ	141	23	04.5
360°			-03.4 ✓

	SUB	TO	S-3	HI	HS
				1351mm	1583mm
ZD	91	52	36.3	4432'	5194'
R	268	07	26.5		
S			2.8	✓	
@	91	52	34.9	✓	
SD	928.425				
Z*M	88	07	29.9		
Z*M	91	52	30.1		

HZD 927.929

DAT. EL 7202 583

	OSCAR	SUB	S-4		
1		06	13.7		
2	210	42	28.9		
1	30	42	33.7		
2	180	06	11.7		
S			6.8	✓	
@	210	36	18.6	✓	
ADJ	210	36	21.7		
1		05	21.2		
2	149	28	59.6		
1	329	28	59.4		
2	180	05	23.9		
S			2.7	✓	
@	149	23	38.4	✓	
ADJ	149	23	38.3		
360°			-04.8	✓	
	SUB	TO	S-4	HI	HS
Z D	90	22	54.7	1351mm	1761mm
R	269	37	01.1	4 432'	5 778'
S			4.2	✓	
@	90	22	56.8	✓	
SD	1360.080				
Z & M	89	37	06.2	and 90	22 53.8
HZ. D	1360.050				
DAT. EL	7223 339				

OSCAR - SUB - S-5

1	0	03	20.6	
2	210	47	10.3	
1	30	47	11.9	
2	180	03	20.3	
S			1.9	✓
@	210	43	50.7	✓
ADJ	210	43	49.3	
1		03	05.7	
2	149	19	20.6	
1	329	19	22.2	
2	180	03	10.6	
S			3.3	✓
@	149	16	13.3	✓
ADJ	149	16	10.7	
360°			+03.9	✓

	SUB TO S-5			HI	HS
				1351mm	1697mm
ZD	89	26	17.3	4 432'	5 568'
R	270	33	38.3		
S			4.4	✓	
@	89	26	19.5	✓	
SD.	1835.385				
Z & M	89	26	14.0	and 90	33 46.0
HZ. D.	1835.295				
DAT. EL	7250 666				

VERT. ∠ @ F.S

	SUB ∠	TO	OSCAR	HS
Z D	79	05	53.8	1368mm
R	280	53	56.0	4 488
S			-10.2	✓
@	79	05	58.9	✓

	S-1∠	TO	SUB	HS
D	78	30	15.5	1565mm
R	281	29	39.3	5 139
S			-05.2	✓
@	78	30	18.1	✓

	S-2∠	TO	SUB	HS
D	85	33	52.6	1815mm
R	274	25	59.8	5 955
S			-07.6	✓
@	85	33	56.4	✓

	S-3∠	TO	SUB	HS
D	88	07	33.3	1583mm
R	271	52	23.9	5 194
S			-02.8	✓
@	88	07	34.7	✓

	S-4∠	TO	SUB	HS.
D	89	37	05.9	1761mm
R	270	22	47.6	5 778
S			-06.5	✓
@	89	37	09.2	✓

	S-5∠	TO	SUB	HS
D	90	33	46.6	1697mm
R	269	26	03.5	5 568
S			-09.9	✓
@	90	33	51.5	✓

1980 (FIELD NOTES)
LEVEL CIRCUIT

BEAR CAN. TO WHITMORE
DAM— DATUM NOT
ASSIGNED

BRIAN ALLRED & MIKE OLSON 6/10/86

STA.	BS+	HI	FS-	IFS	ELEV.	SPAD	DIST.				
RB-1	7.57					5-10-00	0+00				
			1.982								
TP-1	15.41										
RB-2			11.685			5-10-01	5+00				
				0.91							
TP-2	11.605										
RB-3			5.435			5-10-02	10+00				
				1.375							
TP-3	13.599										
RB-4			5.729			5-10-03	16+00				
				0.768							
TP-4	12.47										
RB-5			3.785			5-10-04	20+00				
				1.326							
TP-5	19.263										
			0.945								

STA	BS+	HI	FS-	IFS	ELEV.	SPAD	DIST.				
TP-6	13.081										
RB-6			5.599			S-10-05	25+00				
				0.630							
TP-7	20.74										
			0.89								
TP-8	8.388										
RB-7			6.231			S-10-06	30+00				
				4.443							
TP-9	2.342										
RB-8			4.068			S-10-07	35+00				
				3.975							
TP-10	17.319										
RB-9			8.813			S-10-08	40+00				
				0.153							
TP-11	2.121										
RB-10 SAME STATION	—		6.92			S-10-09	45+00				
TP-12	15.551							BACKSIGHT TO RB			

STA	BS+	HI	FS-	IFS	ELEV	SPAD	DIST.
			2.14				
TP-13	5.459						
RB-11			4.105			S-10-10	50+00
				1.311			
TP-14	12.30						
RB-12			3.089			S-10-11	55+00
				0.92			
TP-15	10.62						
			1.089				
TP-16	7.621						
RB-13			6.631			S-10-12	60+00
				0.15			
TP-17	15.211						
			1.656				
TP-18	9.024						
RB-14			0.03			S-10-13	65+00
				0.75			

STA	BS+	HI	FS-	IFS	ELEV	SPAD	DIST.				
TP-19	13.039										
			0.689								
TP-20	19.79										
RB-15			8.085			S-10-14	70+00				
				0.772							
TP-21	18.149										
			0.521								
TP-22	17.449										
RB-16			9.681			S-10-15	75+00				
				0.122							
TP-23	14.374										
RB-17			5.982			S-10-16	80+00				
				1.015							
TP-24	15.557										
RB-18			2.845			S-10-17	85+00				
				0.842							
TP-25	9.881										

STA	BS +	HI	FS -	IFS	ELEV.	STA	DIST.				
RB-19			2.64			5+10+18	90+00				
				3.37							
TP-26	7.284										
RB-20			3.758			5-10-19	95+00				
				1.564							
TP-27	12.879										
			0.685								
TP-28	8.504										
RB-21			6.505			5-10-20	100+00				
				1.563							
TP-29	11.198										
RB-22			3.358			5-10-21	105+00				
				3.598							
TP-30	18.24										
RB-23			2.445			5-10-22	110+00				
				0.439							
TP-31	7.668										

STA.	BS+	HI	FS-	IFS	ELEV	SPAD	DIST.				
			1.214								
TP-32	11.58										
RB-24			9.588			S-10-25	115+00				
				1.628							
TP-33	8.271										
RB-25			4.198			S-10-24	120+00				
TP-34	8.698						BACKSIGHT TO RB				
			0.403								
TP-35	6.261										
RB-26			4.274			S-10-25	122+45	LAST BOLT			
TP-36	1.253					BACKSIGHT TO ROOF BOLT		RETURN LOOP ↓			
RB-25			11.469								
TP-37	4.395										
			15.023								
TP-38	0.495										
			13.056								
TP-39	0.377										

STA	BS+	HI	FS-	IFS	ELEV.					
			14.252							
TP-40	5.103									
RB-22			6.091							
TP-40	2.316						BACKSIGHT TO		ROOF BOLT	
			13.288							
TP-41	0.65									
			13.965							
TP-41	0.403									
RB-20				5.280			ELEV.	CHECK		
			8.832							
TP-42	3.363									
			8.755							
TP-43	1.031									
RB-18				4.122			ELEV.	CHECK		
			15.996							
TP-44	0.181									
			14.864							

STA	BS+	HI	FS-	IFS	ELEV.	NOTE
TP-45	0.285					
RB-16			9.354			
TP-46	0.710					BACKSIGHT TO RB
			18.712			
TP-47	0.080					
			19.470			
TP-48	0.483					
			14.655			
TP-49	0.401					
RB-14				4.853		ELEV. CHECK
			12.661			
TP-50	0.445					
			14.143			
TP-51	1.209					
			16.39			
TP-52	2.668					
RB-12				7.088		ELEV. CHECK

STA.	BS+	HI	FS-	IFS	ELEV.	
			12.279			
TP-53	1.128					
			9.699			
TP-54	5.365					
			14.355			
TP-55	0.127					
RB-10			4.135			
TP-56	7.151					BACKSIGHT TO RB
			3.685			
TP-57	0.909					
			13.238			
TP-58	0.048					
			5.081			
TP-59	8.080					
RB-8			"	6.631		ELEV CHECK
			6.279			
TP-60	1.581					

STA.	BS+	HI	BS-	IFS	ELEV					
			15.315							
TP-61	0.485									
RB-6			17.735							
TP-62	2.775					BACKSIGHT TO RB				
			19.945							
TP-63	0.401									
			12.181							
TP-64	0.485									
RB-4			13.464							
TP-65	1.823					BACKSIGHT TO RB				
			11.825							
TP-66	2.182									
			11.078							
TP-67	0.576									
RB-2			10.565							
TP-68	2.05					BACKSIGHT TO RB				
			10.165							

STA	BS+	HI	FS-	IFS	ELEV.					
TP-69	4.025									
			4.986							
TP-70	6.640									
RB-1			6.878							
						6/13/86		BRIAN ALLRED MIKE OLSON		SUNNY HOT
RB-16	0.728	344.876			344.148	RE-DO	FROM	RB-16	TO	RB-1
			9.208							
TP-1	1.97	337.638								
			10.842							
TP-2	0.046	326.842								
			16.741							
TP-3	0.057	310.158								
			12.508							
TP-4	1.233	298.883								
			8.071							
TP-5	0.421	291.253								
RB-14				3.092	288.141					

STA	BS	HI	FS	IFS	ELEV
			12.958		
TP-6	1.205				
			11.109		
TP-7	0.328				
			12.378		
TP-8	0.961				
			7.628		
TP-9	0.835				
RB-12			4.078		246.411
TP-10	0.783				
			8.882		
TP-11	2.670				
			7.340		
	4.848				
RB-11				4.077	234.413
			8.038		
TP-12	1.363				

STA	BS+	HI	FS-	TFS	ELEV.
			11.65		
TP-13	1.989				
RB-10				2.497	29.657
			3.995		
TP-14	10.694				
			6.535		
TP-15	0.365				
			13.409		
TP-16	1.408				
			6.745		
TP-17	8.149				
RB-8			4.938		207.198
TP-18	7.655				
			5.535		
TP-19	4.389				
			7.70		
TP-20	0.50				

STA.	BS	HI	FS	IFS	ELEV
			17.861		
TP-21	0.523				
RB-6			12.005		180.764
TP-22	4.110				
			12.805		
TP-23	0.260				
			12.966		
TP-24	0.851				
			8.225		
TP-25	0.787				
			10.506		
TP-26	1.969				
RB-4				5.377	138.252
			9.54		
TP-27	1.758				
			9.273		
TP-28	2.489				

STA	BS	HI	FS	IFS	ELEV.
			8.955		
TP-29	0.66				
			11.556		
TP-30	2.23				
RB-2				2.595	109.389
			8.805		
TP-31	2.945				
			6.364		
	5.401				
RB-1			5.079		100.082