



Canyon Fuel Company, LLC
Soldier Canyon Mine
P.O. Box 1029
Wellington, Utah 84542
(435) 637-6360 Fax: (435) 637-0108

COPY

0003

April 4, 2003

Ms. Pamela Grubaugh-Littig
Department of Natural Resources
Division of Oil, Gas and Mining
1594 West North Temple
Suite 1210
Salt Lake City, UT 84114-5801

RE: Chapter 5 and Reclamation Bond Amendment, Canyon Fuel Company, LLC,
Soldier Canyon Mine, C/007/018

Dear Ms. Grubaugh-Littig:

Enclosed please find four copies of the submittal to address the removal of references made to a refuse disposal site for the Soldier Canyon Mine in Chapter 5 and changes in the bond to reflect the removal of both a refuse site and a preparation plant. In addition the bond has been rewritten in the preferred format.

An additional copy of the submittal has been delivered to the Price Field Office.

Please contact Vicky Miller at (435) 636-2869, if there are any questions concerning this submittal.

Sincerely yours,

Vicky S. Miller

Cc: Chris Hansen (no enclosures)
Dave Spillman (enclosures)
Price Field Office (enclosures)

File in:

Confidential

Shelf

Expandable

Refer to Record No

0003 Date 04042003

In C 0070518 2003 Incoming
For additional information

RECEIVED

APR 04 2003

DIV. OF OIL, GAS & MINING

CANYON FUEL COMPANY, LLC

**SOLDIER CANYON MINE
CHAPTER 5 AND BOND AMENDMENT
C/007/018**

APRIL 2003

TABLE OF CONTENTS

<u>NUMBER</u>	<u>DESCRIPTION</u>	<u>PAGE</u>
CHAPTER 5	ENGINEERING	5-1
5.10	Introduction	5-1
5.11	General Requirements	5-1
5.12	Certification	5-1
5.12.25	Primary Roads	5-1
5.13	Compliance with MSHA Regulations & MSHA Approvals	5-1
5.14	Inspections	5-2
5.15	reporting and Emergency Procedures	5-2
5.20	Operations	5-3
5.21	General	5-3
5.21.11	Previously Mined and Presently Mined Areas	5-3
5.21.12	Existing Surface and Subsurface Facilities and Features	5-3
5.21.13	Landowners and Right-Of-Entry and Public Interest Maps	5-3
5.21.14	Mine Maps and Permit Area Maps	5-4
5.21.15	Land Surface Configuration Maps	5-4
5.21.16	Maps and Cross-section of the Features and Proposed Features	5-4
5.21.17	Transport Facilities Maps	5-4
5.21.20	Signs and Markers	5-5
5.22	Coal Recovery	5-5
5.23	Mining Methods	5-7
5.24	Blasting and Explosives	5-17
5.25	Subsidence	5-17
5.25.10	Subsidence Control Plan	5-17
5.25.11	Methods of Coal Removal	5-21
5.25.12	Description of Physical Conditions	5-23
5.25.13	Measures to Prevent Subsidence	5-23
5.25.14	Monitoring	5-25
5.25.16	Mitigation of Damages	5-28
5.25.20	Subsidence Control	5-28
5.25.30	Public Notice of Proposed Mining	5-29
5.25	Refuse Disposal Site	5-29
5.26	Mine Facilities	5-29
5.26.20	Utility Installations & Support Facilities	5-34
5.26.21	Utility Installations	5-34
5.26.22	Support Facilities	5-36
5.26.3	Water Pollution Control	5-42
5.26.4	Air Pollution Control	5-43
5.27	Transportation Facilities-Road Classification	5-43
5.27.2	Transportation Facilities	5-46
5.28	Handling and Disposal of Coal, Overburden, Excess Spoil, and Coal Mine Waste	5-47
5.29	Management of Mine Openings	5-49
5.30	Operational Design and Plans	5-49
5.31	General	5-49
5.32	Sediment Control	5-49
5.33	Impoundments	5-49
5.34	Roads	5-50

TABLE OF CONTENTS (Continued)

<u>NUMBER</u>	<u>DESCRIPTION</u>	<u>PAGE</u>
5.35	Spoil	5-52
5.36	Coal Mine Wastes	5-53
5.37	Regraded Slopes	5-53
5.37.10	Geotechnical Analysis	5-53
5.37.20-25	Regrading of Fills	5-53
5.40	Reclamation Plan	5-53
5.41	General	5-53
5.41.10-40	Permanent Closure of all Facilities	5-53
5.42	Narratives, Maps and Plans	5-54
5.42.10	Timetable	5-54
5.42.20-32	Final Surface Configuration	5-54
5.42.40	Bond Release	5-63
5.42.50	Sedimentation Ponds	5-63
5.42.60-63	Roads	5-63
5.42.70-71	Mine Openings	5-64
5.42.72-74	Disposal of Spoil and Waste	5-65
5.42.80	Estimate of Reclamation Costs	5-65
5.50-5.51	Sealing of Underground Openings	5-70
5.52-52.20	Permanent Features	5-70
5.53-53.24	Backfilling and Grading	5-70
5.53.25-42	Refuse Piles	5-70
5.53.60-65	Approximate Original Contour	5-71
5.53.70-83	Surface Coal Mining Reclamation Activities	5-71
5.53.90	Regrading of Settled and Revegetated Fills	5-71
5.60	Performance Standards	5-71

CHAPTER 5

ENGINEERING ~~{R614-301-500}~~

5.10 Introduction

This chapter presents designs, maps, plans and cross-sections of the facilities and structures required to minimize the potential impacts of the Soldier Canyon Mine operations. ~~This permit was written using R614-301-500 regulations, therefore the format does not follow the order of the R645-301-500 regulations.~~

5.11 General Requirements

The methods, calculations, maps, plans and cross-sections attendant to the operations of the Central Mine Facilities ~~and proposed refuse disposal site~~ and the subsequent reclamation operations are presented in the following sections. These designs are required to comply with the design in R614-301-500 regulations.

5.12 Certification

SCCC provides, in this permit application, certified cross-sections and maps of surface facilities, hydrologic structures, geologic resources, plans and engineering designs ~~for coal mine refuse areas, impoundments, and primary roads applicable to the proposed refuse disposal area.~~

5.12.25 Primary Roads

I, J.T. Paluso, being a professional engineer licensed in the State of Utah, License Number UT-4028, due hereby certify that the design and construction or reconstruction of primary roads as described in the plan meet the requirements of R645-301-534.200 and R645-301-742.420.

5.13 Compliance with MSHA Regulations and MSHA Approvals

~~The design for the refuse disposal area will meet the MSHA requirements as specified in 30 CFR 77.214 and .215.~~ Soldier Creek Coal Company will comply with

the requirements of both DOGM and MSHA regarding these facilities.

5.14 Inspections

All engineering inspections, except those described under R614-301-514.330, will be conducted by a qualified registered professional engineer or other qualified professional specialist under the direction of the professional engineer.

~~Refuse pile inspections will be performed by a professional engineer or an engineering specialist, under the supervision of a professional engineer, during placement and compaction of coal mine waste materials. More frequent inspections will be conducted if a danger or harm exists to the public health and safety or the environment. Inspections will continue until the refuse pile has been finally graded and revegetated or until a later time as required by the Division.~~

~~Such inspections will be made at least quarterly throughout construction and during the following critical construction periods:~~

~~Foundation preparation including the removal of all organic material and topsoil,~~

~~Installation of final surface drainage system, and~~

~~The final graded and revegetated facility.~~

~~The qualified registered professional engineer will provide a certified report to the Division promptly after each inspection that the refuse pile has been constructed and maintained as designed and in accordance with the approved plan and R614 rules. The report will include appearances of instability, structural weakness, and other hazardous conditions.~~

~~A copy of each inspection report will be retained at the Soldier Canyon Mine site.~~

Sediment pond and sewage lagoon inspections will be performed quarterly by a qualified person for appearance of structural weakness and other hazardous conditions. These structures will also be inspected at least yearly, until

removal or release of the performance bond, by a professional engineer and a certified inspection provided to the Division. These inspections will meet the requirements of R645-301-514.300.

A copy of each inspection report will be retained at the Soldier Canyon Mine site.

5.15 Reporting and Emergency Procedures

At any time a slide occurs which may have a potential adverse effect on public, property, health safety or the environment, Soldier Creek Coal Company (SC3) will promptly contact the Division and inform the Division of the problem and of any remedial measures planned. Similarly, if the inspections of the ~~refuse pile~~, sediment ponds, and sewage lagoon disclose a potential hazard, SC3 will promptly notify the Division of the problem and of any remedial measures planned to alleviate the problem.

In the event of a temporary cessation of the Soldier Canyon Mine operation, SC3 will notify the Division as soon as possible and will effectively support and maintain all surface access openings to underground operations, and secure surface facilities in areas in which there are no current operations, but operations are to be resumed under an approve permit.

Before temporary cessation of coal mining and reclamation operations for a period of 30 days or more, or as soon as it is known that a temporary cessation will extend beyond 30 days, Soldier Creek Coal Company will submit to the Division a notice of intention to cease or abandon operations. This notice of the Division will be as required by R614-301-515-321.

5.20 Operations

This section presents the operations plan for the Soldier Canyon Mine operations.

5.21 General

This section presents a description of the plan for operation of the central mine

facilities and topsoil site ~~and refuse disposal site~~. The general layout of the various facilities for the Soldier Canyon Mine operations are presented on Exhibits 5.21-1, 5.21-2 and Plate 5-1. Maps, cross-sections, and calculations for the specific facilities are presented to support the narrative description. The Applicant will not conduct mining activities outside the approved permit area, and any mining activity conducted within the permit area will not affect areas outside the permit area boundary.

5.21.11 Previously Mined and Presently Mined Areas

Exhibits 5.22-1 and 5.22-2 show the location and extent of past and present underground mining operations.

5.21.12 Existing Surface and Subsurface Facilities and Features

The location of all buildings in and within 1000 feet of the permit area; the location of surface and subsurface man-made features within, passing through, or passing over the permit area; each public road located in or within 100 feet of the permit area; and the location and size of the sewage lagoon, and topsoil storage site ~~and proposed refuse disposal site~~ are shown on Exhibits 1.12-1, 5.21-1, 5.21-2, 5.26-1 and Plate 5-1. REI's power line is shown on Exhibits 5.21-1 and 5.25.1

5.21.13 Landowners and Right-of-Entry and Public Interest Maps

Exhibits 1.12-1, 1.12-2, 5.21-1, 5.21-2, Plate 5-1 and Figure 5.26-1 show the owners of record of those lands both surface and subsurface, included in or contiguous to the permit area; the boundaries of land within the proposed permit area upon which the applicant has the legal right to enter and begin coal mining and reclamation operations; and the measures to be used to ensure that the interests of the public and landowners are protected as required under R614-103-234 when conducting coal mining and reclamation activities, within 100 feet of the right-of-way line or relocating a public road.

5.21.14 Mine Maps and Permit Area Maps

Exhibits 5.21-3, 5.21-4 through 5.21-8, 5.25-1 and Plate 1 show the boundaries of all areas proposed to be affected over the estimated total life of the coal mining and reclamation operations, sequence and timing of the mining of subareas for which additional permits will be sought, the coal mining and reclamation operations to be conducted, the lands to be affected throughout the operation and any change in a facility or feature to be caused by the Soldier Canyon Mine operations. Also, the underground workings and location and extent of areas where subsidence is planned and where measures will be taken to prevent, control or minimize subsidence-related damage.

5.21.15 Land Surface Configuration Maps

Topographic maps used by the Applicant clearly indicate surface contours to adequately represent the existing land surface configuration within the permit area.

5.21.16 Maps and Cross-sections of the Features and Proposed Features

Maps produced by the Applicant will show the facilities, disturbed area, disturbed area boundary, explosive storage and point source discharges for their specific requirement are included within this application.

5.21.17 Transportation Facilities Maps

This application describes each road and conveyor system to be constructed and used by the Applicant as required by R614-301-527.

5.21.20 Signs and Markers

Signs and markers will be posted, maintained, and removed by the operator; will be a uniform design that can be easily seen and read; be made of durable material; and conform to local laws and regulations; and be maintained during all activities to which they pertain.

These signs shall include a mine and permit identification sign, perimeter markers, buffer zone, and topsoil markers.

5.22 Coal Recovery

Conservation of Coal Resources

The Bureau of Land Management (BLM) and the Utah Division of State Lands & Forestry govern the conservation and royalty payments of the coal located within Applicant's proposed permit boundary. Mining plans for all seams must be approved by the BLM (43 CFR 3480 et al) and the Utah Division of Oil, Gas & Mining (Regulatory Authority) before mining can occur within the new area. This prior approval ensures the diligent development and extraction of all minable coal.

Three coal seams within the LOM area, the Sunnyside, the Rock Canyon, and the Gilson, will be mined (Exhibits 5.21-4, -5 and -6). The underground operations have been planned to yield the maximum recovery of the coal reserves using the safety of mine personnel, accepted economic mining practices, and the protection of the environment as criteria. In addition, product quality, as it pertains to present and future customer needs, was also used as a secondary criterion in planning. The plans anticipate increasing current production rates so that longwall mining can be introduced to supplement the current room and pillar operations. Adherence to these guidelines will improve mining conditions in each seam and aid in the maximum, safe recovery of the individual coal horizons. In the event that future mining technology (not yet developed) is more efficient than present technology and is compatible with the Applicant's mining operation, then these new technologies will be applied to the extraction of Soldier Canyon coal.

Although maximum recovery is an important design criteria, other factors must also be considered to ensure the protection of personnel and the environment. Coal reserves will not be recovered in the following areas:

1. Areas where the coal is less than 5 ft thick will not be mined as

mining in that height is not feasible under current economic conditions.

2. Coal will only partially be mined in the immediate vicinity of shafts, portals, or any connections between seams. This will prevent subsidence and protect structures in those areas.
3. Solid coal barriers will be left intact to protect the main entries from mined out panels.
4. Solid coal barriers will be left between certain panels for roof and floor protection and to provide seal areas in the event of a fire or gas accumulation.
5. Solid coal barriers of required size will be left along the property boundaries as required by the General Safety Orders of Utah and or BLM.
6. To minimize the chances of exposure to dangerous quantities of harmful gases or flooding of the working sections, solid coal barriers of sufficient size will generally be left around old workings.
7. In most cases, main, barrier, bleeder, and longwall panel pillars will not be recovered because of the extreme hazards associated with such recoveries.
8. Due to the minimal amount of interburden between the Rock Canyon and Gilson seams (< 30 ft a locations) only one seam may be mined in specific areas. This is because of the dangers associated with mining both seams under these conditions.
9. Coal will only partially be recovered in areas below and adjacent to the Soldier Creek drainage channel. This is for protection of surface features and facilities as described in Section 5.25.

Maximum Economic Recovery

Utilization of room and pillar and longwall mining methods will make maximum coal recovery more feasible because the mining operations will be more versatile to meet diverse mining conditions. The mine layout is designed to maximize the number of longwall panels and to minimize waste of coal reserves near the boundaries of the property.

Annual Production

Maximum annual production will not be reached until the year 1998. However, the maximum production rate for the mine will begin in 1994 and continue for approximately nine years (Table 5.22-1). At the end of this period, annual tonnage will decline until the various mine reserves have been depleted. During full production periods, the mine will experience variations in annual tonnage. This is due to the moving of the longwall section more than once during the year.

~~The Applicant maintains three work shifts per day. The labor force is anticipated to expand from approximately 120 to 160 miners and staff when maximum annual production is obtained. The average number of working days per year is 252. The Applicant presently employs 101 hourly and 33 salaried personnel.~~

Life of Mine

The life of the mine is subject to the size and geometry of the reserves, and the rate at which the reserves are mined. The projected life of the mine is shown in Table 5.22-1.

5.23 Mining Methods

Mine Plans and Layout

In 1989 J.F.T. Agapito & Associates, Inc. were contracted to evaluate and design a three-seam longwall layout for the Soldier Canyon Mine. This study consisted of executing the following activities: 1) Site Selection and Inspection of Surface Resources, 2) Instrumentation and Data Analysis, 3) Three-seam Gate Design, 4) Subsidence Evaluation, 5) Develop a Mine Plan Layout for Efficient Three-seam Extraction, 6) Develop a Ventilation Plan for the Proposed Mine Layout, and 7) Presentation of Results/Final Report. This final report, Mine Layout design and Ventilation Analysis for Soldier Creek Coal Company, is presented as Appendix 5-D and now forms the basis for the present mine plan. This proposed mine layout has provided the best compromise solution for stability, resource recovery, ventilation, haulage, production requirements and protection of surface resources. The following parameters were concluded:

Direction of Mining - Based on the cleat/joint measurements and stress measurement in the existing mine an east-west and north-south orientation was selected as the preferred direction of mining. This orientation provides the best compromise for roof and rib stability.

Table 5.22-1

Forecasted Average Annual Coal Production
 Soldier Canyon Mine
 1991 - 2009
 (000's tons)

Year	Continuous Miners			Longwall	Total
	Unit A	Unit B	Unit C		
1991	504	504	192	-	1,200
1992	504	277	419	-	1,200
1993	504	185	-	1,500	2,189
1994	504	234	-	2,320	3,058
1995	504	184	-	2,270	2,958
1996	504	233	-	2,320	3,057
1997	504	171	-	2,320	2,995
1998	504	185	-	2,420	3,109
1999	504	229	-	2,320	3,053
2000	504	237	-	2,320	3,061
2001	504	277	-	2,270	3,051
2002	504	277	-	2,320	3,101
2003	-	277	-	2,320	2,597
2004	-	140	-	2,420	2,560
2005	-	140	-	2,320	2,460
2006	-	277	-	2,320	2,597
2007	-	277	-	2,220	2,497
2008	-	114	-	2,320	2,434
2009	-	-	-	1,245	1,245
Totals	6,048	4,218	611	37,545	48,422

Panel Retreat Sequence - It is proposed that longwall panels be extracted from the top of the seam toward the bottom. This is referred to as "Downdip" panel retreat. While an updip retreat is beneficial for overall roof stability, the downdip was selected for methane control. This downdip retreat direction will enhance methane movement in an updip direction, away from the longwall face.

Multiple-Seam Workings Position - The proposed mine layout calls for all mains to be directly columnized. Columnization will be most important for mains, submains and bleeders in the Rock Canyon and Gilson seams due to the minimal interburden. Longwall panel gate road development will, however, be offset. Offsetting of gate pillars under the gob of the upper seam will improve the lower seam gate stability.

Longwall Panel Dimensions - The longwall dimensions selected for the mine layout range from 610 to 680 ft. wide and from 3,800 to 5,700 ft. long.

Longwall Panel Gate Road development - A two-entry, yield pillar system was selected for gate road development. This design was based on an overall evaluation of the depth of cover, cleated nature of the coal seams, thickness of coal seams, roof rock strengths and multiple-seam mining plans.

Recommended Pillar Designs - Utilizing the in-mine stress measurements, as well as an evaluation of roof, coal and floor strength properties, recommended pillar dimensions were designed for different depths. The recommended pillar designs are presented in Table 5.23-1.

Pillar Extraction

Full pillar extraction in room and pillar areas will be performed in accordance with the current approved mining plan. This provides for the recovery of the reserves in those areas by a proven method. Extraction of coal in longwall areas will be performed on panels approximately 680 ft. in width and from 3,800 to 5,700 ft. in length. The panel layout also provides for modifications should future technology develop a safer method of development or extraction.

Bleeder entries will generally be driven around all areas where full extraction, either by longwalls or continuous miners, is to take place.

Table 5.23-1
Recommended Pillar Designs
(Agapito 1991)

Cover (Ft.)		Depth of
2250	2500	1500 2000

Main Development		
Pillar spacing center-to-center (ft.)		80 by 80 100 by 100
100 N/A 120 by 120		
Recommended number of entries		6 5
N/A 4-5		

Barrier Pillars		
Recommended Pillar Widths (ft.)		250 300
N/A 350		

Gate Pillars-Sunnyside seam		
Pillar spacing center-to-center (ft.)		N/A 54 by 118
54 by 138 58 by 138		
Recommended Entry spans (ft.)		18 18
18 18		

Gate Pillars-Rock Canyon seam		
Pillar Spacing center-to-center (ft.)		N/A 56 by 120
56 by 140 N/A		
Recommended Entry spans (ft.)		N/A 18
18 N/A		

Gate Pillars-Gilson seam		
Pillar Spacing (East Block) (ft.)		N/A N/A
53 by 138 N/A		
Pillar Spacing (North Block) (ft.)		N/A N/A
N/A 58 by 138		
Pillar Spacing (West Block) (ft.)		N/A 46 by 118
N/A N/A		
Recommended Entry spans (ft.)		N/A 18
18 18		

Longwall Mining

The mine layout maximized the number of panels, especially longwall panels. Main entries, submains, and panels have been aligned to minimize the waste of coal reserves near property boundaries and areas of thin coal. Coal will be mined from a longwall face approximately 680 ft. wide by a double ranging drum shear.

Longwall panels will be developed using a 2 entry system. This provides for a yield pillar, and in conjunction with the cribbing of the tailgate entry prior to longwall mining will give adequate roof control to enable safe extraction of the coal.

Multi-Seam Considerations

In order to ensure the maximum recovery of coal from all minable seams and to avoid hazardous mining conditions, the Applicant will adhere to the following guidelines during multiple seam mining operations:

- a) Coal will be mined from top to bottom in accordance with standard descending seam extraction practices.
- b) Where possible, mining in the upper seam will precede mining in the seam immediately below it by at least one year. This staggering of operations will allow time for the overburden to settle and stabilize before mining begins in the lower seam.
- c) The protective barrier pillars for all main and submain slope entries, main haulageways, primary air courses, bleeder entries, and manways in each seam shall be superimposed whenever possible, regardless of vertical separation or rock competency.

Shafts and Interconnection of Rock Slopes

The Sunnyside and Gilson seams will be accessed through rock slopes driven from the Rock Canyon seam. In each case, an adequate number of airways will be driven from the Rock Canyon seam, as well as one beltway. The intake airway will also be used to transport men and supplies. The exact number, size and location will be determined according to mining conditions and MSHA approved roof control and ventilation plans.

Ventilation System

A detailed description of the ventilation system as well as an explanation of the methane and dust control plan is routinely reviewed and approved by MSHA. The ventilation system was designed to provide a dependable, adequate supply of uncontaminated air to all underground work areas. Air volume and velocity are sufficient to dilute, render harmless and carry away flammable, explosive or toxic gases as well as dust, gases generated by explosives, smoke and fumes.

Two Joy Axivane exhaust fans provide adequate volumes of fresh air to the work areas. Fan No. 1, powered by a 500 hp (440 V) motor, is capable of moving 450,000 cfm. Fan No. 2, with an 800 hp (4160 V) motor is presently producing 645,000 cfm. Both fans are equipped with auxiliary diesel engines.

Roof Control Plan

Roof control is based on a full bolting plan: conventional supplemental materials and supports are used as needed. The plan was reviewed by MSHA and subsequently approved.

When adverse roof conditions are encountered, spot bolting is used to supplement the conventional roof control plan. In areas where spot bolting is deemed necessary, either resin or conventional roof bolts are installed on four-foot centers. Spot bolting begins in competent roof and continues until competent roof is again encountered. If necessary, wire mesh matting or rib bolts are installed in main headings to maximize the stability of these entries. All conventional bolting materials are chosen, installed, and positioned in accordance with 30 CFR 75.200-7 (a) and (b), 75.200-8, and 75.200-10.

Hydraulic props with ropes, timbers or cribs are used as breaker rows and turn props during pillar extraction. Pillar splitting procedures are in accordance with 30 CFR 75.200-11.

Projected Mine Development

Detailed maps of all three seams showing the development of the mine are presented on Exhibits 5.21-4, -5 and -6. The proposed mine plan expands the present Soldier Canyon operation from the Rock Canyon seam to include the Sunnyside and Gilson seams. The present room and pillar methods will be

supplemented with a longwall unit.

Mine Water System

Pumps ranging in size from 5 to 400 hp, using pipes 2 in. to 8 in. in diameter control incoming formation water. Water not used for dust suppression in the mine is released to Soldier Creek under authorization of NPDES Permit No. UT-0023680. Waste water is gravity fed into two sewage lagoons located 2 miles from the mine site.

When mine water is encountered, it is channeled by the natural pitch of the seam to the low areas, and from there is pumped into an underground sump. Water in the sump is used either for dust suppression in the mining sections or, after most of the suspended solids have settled out is pumped out of the mine into Soldier Creek under authority of NPDES Permit No. UT-0023680.

Hazardous Wastes

It is not anticipated that acid-forming or toxic waste will be discovered during mining. However, if these conditions are encountered, the Regulatory Authority will be notified and a plan will be developed and submitted to the Agency for approval.

Equipment

The machinery for the mine is equipped, maintained, and operated to ensure maximum safety, productivity, and quality of coal production. All underground equipment is approved by MSHA. Table 5.23-2 lists the major underground and surface equipment to be used. These lists are not exclusive and equipment design and choices may vary during the course of mining.

All pieces of stationary and mobile equipment at the mine are assigned a projected useful service life and depreciated accordingly. If the depreciation life of a particular unit expires and the equipment is still in serviceable condition with acceptable availability and maintenance costs, the service life is extended.

Mining equipment abandoned underground due to unsafe recovery conditions has been drained of lubricants and other potentially hazardous fluids to the extent

possible. The location of the equipment is illustrated on Exhibit 5.22-1.

Mine Safety

The Applicant considers attention to health and safety of each miner to be a prime contributor to the continued success of the mining operations. The Applicant complies with all MSHA and State of Utah health and safety laws to protect the well-being of its employees. A number of safety provisions have been incorporated into the proposed mining operations to ensure compliance with those laws.

Safety Training

The mine is equipped with modern emergency facilities and has an organized, functioning safety program. All mine employees are instructed concerning mine safety procedures and meet MSHA first aid and safety training requirements. New employees are required to attend a minimum of 40 hrs. of classroom orientation before starting work in the mine.

Fire Protection

In the event of a surface facility or mine fire, the water storage tank located on the surface and underground water sumps will be used to provide water necessary to control the fire. Water lines from the underground sumps are aligned along conveyor belt lines leading to each working face. Outlets have been installed along the water line for quick and easy access in case of any emergency. Fire hydrants and fire extinguishers are strategically located to ensure the protection of all personnel and the environment.

Water or chemical deluge systems with sprays are located at the belt drives to prevent mine fires. Fire extinguishers in operable condition are provided for all structures and equipment where they may be a potential fire hazard. All underground equipment complies with state and federal regulations and is well maintained.

Additional measures are taken to prevent mine fires. All combustible materials are so stored to minimize the potential for combustion. Suitable fire-fighting equipment is provided and trained personnel are certified to use breathing apparatus in case of a mine fire or rescue. Smoking or the carrying of any type

of open flame device is prohibited in the mine and within 25 ft of the portals. These portal areas are designated fire lanes.

Each mine operation complies with the fire protection requirements outlined in MSHA regulations, 30 CFR Parts 75 and 77. A copy of MSHA's approval of plans for extinguishing potential waste fires will be submitted to the regulatory authority upon request.

Mine waste fires will be handled in a manner similar to the mine fire protection system. The system is one of, first protection, and second suppression. Prevention is primarily a safety and training matter dealt with by an ongoing educational program concerning the need for continuous attention to fire prevention. The engineering design for the mine waste disposal areas reduced potential for spontaneous combustion by continuous compaction and covering of material. Second, the suppression system consists of fire extinguishers or fire hoses available for use should a fire develop. Operators are instructed to separate any smoldering material and compact the adjacent material. The burning material is then extinguished by appropriate methods.

Handling of Explosives

The utilization of continuous mining machines and longwall mining machines normally does not require the use of explosives. Some underground construction activities, however, such as the construction of shafts and overcasts, penetration of faulted areas or rock spars, and breaking of fallrock, may require the use of explosives. Explosives are handled in accordance with state and federal laws and are stored, transported and handled by experienced, approved, and certified personnel in accordance with Article VI, Utah General Safety Order of Utah Coal Mines, Section 48 through 53, 30 CFR 75.1300 and the manufacturer's recommendation.

Dust Control

Coal dust is controlled through good housekeeping, wetting face areas, rock dusting, and ventilation. Large quantities of coal dust are prevented from accumulating on the surface of any type of equipment capable of producing heat or sparks. All working areas and return entries are rock dusted to prevent dangerous accumulations of coal dust.

A pipeline system is provided for wetting the rib, roof, and floor surfaces for a distance of at least 40 ft from each working place, except where these areas are naturally wet. In dry working places, the face areas are kept wetted back to where rock dust has been applied.

All mining equipment or operational areas that are subject to large concentrations of dust are equipped with water sprays at the source to keep airborne dust to a minimum.

Within the mine rockdust and continuous water spray at the mine face and transfer points protect the miners from excessive amounts of dust. Monitoring has shown that coal dust content in the air at the working face is 1.2 mg/8 hrs. Haulageways are wetted and/or otherwise treated to assist in dust control.

Adequate ventilation is provided to each working face to quickly remove dust particles during the course of mining. All mine operations comply with MSHA and State of Utah laws to keep respirable dust to a minimum. Dust sampling is done as outlined by MSHA.

Diesel Emissions

Diesel equipment in the mine is used in accordance with all state and federal regulations, including the following:

- 1) Only diesel equipment approved by the Bureau of Mines or MSHA is used underground.
- 2) Diesel equipment is used only in well-ventilated areas.

All measurements and sampling are in accordance with federal and state laws.

5.24 Blasting and Explosives

The Applicant will comply with all state and federal laws in the use of explosives during the construction of the surface facilities expansion, and whenever blasting is required for the Soldier Canyon Mine. A certified blaster will direct all blasting operations with the help of at least one other person. The Applicant will make sure that all contractors working on any project are made aware of the blasting procedures. All blasting records will be kept on file at SCM for the required period of time.

All explosive containers used at the mine are built to meet or exceed the specified requirements set forth by the Mine Safety and Health Administration. The surface storage containers are placed in a position to ensure the protection of the environment and all personnel. Those containers, one for caps and one for powder, are located on the surface on skids and made of 1/4-1/2 inch steel plate with wood lining of 1/2 inch plywood. Two five tumbler locks, adequately protected, are used. Both magazines have two vents measuring approximately 3x3 inches.

The portable container used for the transportation of explosives underground is a small metal utility trailer. The trailer is wood lined with caps and powder kept separate. As required by law, no metal screws or metal parts are exposed.

5.25 Subsidence

5.25.10 Subsidence Control Plan

Surface Features and Facilities Subject to Subsidence, Slides and Other Damage

A survey of the surface area overlaying and adjacent to the proposed mine plan area has been completed. All structures and renewable resource lands, which could conceivably be adversely affected by subsidence or other mining induced surface failure, (e.g. slides, slumps, etc.) have been identified and listed below (also see Exhibit 5.25-1).

- Questar Pipeline Company's 20-inch natural gas pipeline.
- Western Natural Gas, Inc./Resource Enterprises, Inc. (REI) degasification facilities, which include two compressor facilities, one exhaustor/blower facility, four vertical boreholes and associated gas and power lines.
- Carbon County's public road 53.
- The Pine Canyon private road.
- Streams - Soldier Creek and Pine Creek
- Most surface areas are utilized for livestock grazing.

Most of the area subject to possible subsidence is currently used for low-

intensity summer grazing of domestic livestock (primarily cattle and sheep). Subsidence should have no effect on grazing. No other renewable resources exist in this area. The area does, however, have a limited potential for recreational use, such as hunting. Again, subsidence should have no effect on any recreational use.

Existing structures, within the mine plan area, include the Questar natural gas pipeline and the Western Natural Gas, Inc./REI coal bed degasification facilities. The overall subsidence control plan has been designed to ensure that these facilities continue to operate, uninterrupted, and are in no way jeopardized by mining induced subsidence. (See section 5.25.13 Measures to Prevent Subsidence).

One County road passes through the permit area along Soldier Creek. Also, a single dirt road of restricted local use is located along the base of Pine Canyon. The subsidence control plan has been designed so as to prevent any damage to these roads. Subsidence should not damage the roads; however, if damage does occur, it would be slight and easily repaired.

Streams in the life of mine (LOM) area are described in detail in Sec. 7.24.2, Surface Water Information. The nature of subsidence resulting from the proposed mine plan should not significantly affect any streams.

The subsidence control plan has been designed to prevent damage to the streams. Gentry and Abel (1978) demonstrated that topographic lows (such as are the stream beds) are in fact protected in part by "piling up" of the opposite facing ridge slopes (adjacent topographic highs) during actual subsidence events. Therefore, mining induced surface fracturing should be very limited or nonexistent within the stream bed areas and readily filled.

The maximum potential subsidence boundary, which could extend beyond the present five-year term permit area, is detailed on Figure 5.25-1. This subsidence boundary was projected to the surface utilizing an angle of draw of 22.5 degrees. This projection was extended from all coal lease boundaries where a coal seam of mineable thickness exists. In areas where there are multiple seams of mineable thickness, the lower most seam was used for the subsidence projection. Please

note that the maximum potential subsidence boundary was projected independently from the approved mine plan. Therefore, the subsidence projection represents a worst case condition, where full extraction mining would occur up to all existing coal lease boundaries. While a 22.5 degree angle of draw is generally considered a conservative estimate, it was utilized to be consistent with the subsidence evaluation performed by J.F.T. Agapito and Associates, Inc. (contained within the Mine Layout Design and Ventilation Analysis - Appendix 5-D). Since the approved mine plan does not propose full extraction mining up to the coal lease boundaries, a further evaluation at a 35 degree angle of draw was performed. Results indicate that a projection of a 35 degree angle of draw from the proposed full extraction areas will not extend beyond the subsidence buffer zone as detailed. Any future mine plan modifications shall maintain a 35 degree angle of draw projection within the subsidence buffer zone unless one of the following conditions is satisfied.

- The Applicant shall demonstrate to the Division's satisfaction that there is no potential for material damage, environmental harm or damage to human health in the subsided areas.

- The Division shall accept a lesser degree angle of draw, based on detailed analysis and engineering evidence submitted by the Applicant.

In order to permit all areas which could potentially be affected by subsidence, a subsidence buffer zone has been added to the Soldier Canyon Mine Five-Year Term Permit Area (see Figure 5.25-1). This subsidence buffer zone includes approximately 1,473 acres and is included on the U.S.G.S. 7.5 minute quadrangle maps Deadman Canyon and Pine Canyon. A legal description of this additional permit area is as follows:

Township 13 South, Range 11 East, SLB&M:
Section 1: Lots 1,2,5,6 & 7, Section 12: W $\frac{1}{2}$ W $\frac{1}{2}$,
Section 13: NW $\frac{1}{4}$ NW $\frac{1}{4}$.
Township 13 South, Range 12 East, SLB&M:
Section 3: W $\frac{1}{2}$ W $\frac{1}{2}$, Section 10: NW $\frac{1}{4}$ NW $\frac{1}{4}$.
Township 12 South, Range 12 East, SLB&M:
Section 28: SW $\frac{1}{4}$ SW $\frac{1}{4}$, Section 29: S $\frac{1}{2}$ S $\frac{1}{2}$,
Section 30: SE $\frac{1}{4}$ SE $\frac{1}{4}$, Section 31: E $\frac{1}{2}$ E $\frac{1}{2}$,

SW 1/4 SE 1/4, S ½ SW 1/4, Section 32: NW 1/4 NE 1/4,
Section 33: W ½ W ½, SE 1/4 SW 1/4, S ½ SE 1/4,
Section 34: S ½ SW 1/4, W ½ SW 1/4 SE 1/4.

All surface owners, which will be affected by the incorporation of the subsidence buffer zone, have been contacted. Subsidence buffer zone letters were sent to Carbon County, Bureau of Land Management, Questar Pipeline Company, Mrs. Louise Iriart and Newell Nelson on September 1, 1992. Copies of the signed comments can be found in Illustration 5.25-1.

We are presently working with Questar, BLM and Newell Nelson to resolve potential problems. The pending sale of Soldier Creek has made it impossible to accurately define future mine plans. In the near future, when these plans are completed, these areas of concern will be addressed.

Also, as required, a proposed public notice has been prepared for publishing within the Sun Advocate, the local newspaper (see page 5-17d). This public notice will fulfill the requirements for a significant permit revision, as well as, for the proposed mining activities within 100 feet of a public road.

Following approval of the subsidence buffer zone, the Applicant shall modify the appropriate maps within the MRP and surface signs within the permit area to comply with the permit revision.

5.25.11 Methods of Coal Removal

Much of the reserve area will be mined using a longwall system, or full extraction room and pillar methods. As explained by Von Schonfeldt, et al., 1980, "subsidence when uniform rarely causes problems to renewable resources such as aquifers, streams and ranch lands." Therefore, as a result of using full extraction methods the surface above the mine will lower uniformly and no significant fracturing should occur. The slight decrease in the elevation at the surface is not expected to adversely affect any existing structures, stream, or roads.

To date, no significant surface effects due to subsidence in any part of the mine permit area or adjacent areas have been observed, although some surface

subsidence theoretically is expected to occur as a result of historic and current mining activities. The Applicant's proposed mining plan has been designed using technically sound criteria to prevent significant mining induced impact to surface lands or existing structures. The following paragraph of this section describes how the proposed mining procedures will affect subsidence and the extent of controlled subsidence resulting from mining.

(Proposed)

Public Notice
Soldier Creek Coal Company
Soldier Canyon Mine
P.O. Box I, Price, Utah 84501

Soldier Creek Coal Company has submitted to the Utah Division of Oil, Gas and Mining an application for a significant revision to the previously approved Mining and Reclamation Plan (ACT/007/018). Pursuant to R645-300-121.100, public notice is hereby given regarding this proposed permit revision.

In order to protect all areas which could potentially be affected by underground coal mining activities, a subsidence buffer zone is proposed for addition to the Soldier Canyon Mine Five-Year Term Permit Area. This subsidence buffer zone includes approximately 1,473 acres and is contained within the U.S.G.S. 7.5 minute quadrangle maps "Deadman Canyon" and "Pine Canyon". A legal description of this additional permit area is as follows:

Township 13 South, Range 11 East, SLB&M:

Section 1: Lots 1, 2, 5, 6 & 7, Section 12: W $\frac{1}{2}$ W $\frac{1}{2}$,
Section 13: NW $\frac{1}{4}$ NW $\frac{1}{4}$.

Township 13 South, Range 12 East, SLB&M:

Section 3: W $\frac{1}{2}$ W $\frac{1}{2}$, Section 10: NW $\frac{1}{4}$ NW $\frac{1}{4}$

Township 12 South, Range 12 East, SLB&M:

Section 28: SW $\frac{1}{4}$ SW $\frac{1}{4}$, Section 29: S $\frac{1}{2}$ S $\frac{1}{2}$
Section 30: SE $\frac{1}{4}$ SE $\frac{1}{4}$, Section 31: E $\frac{1}{2}$ E $\frac{1}{2}$
SW $\frac{1}{4}$ SE $\frac{1}{4}$, S $\frac{1}{2}$ SW $\frac{1}{4}$, Section 32: NW $\frac{1}{4}$ NE $\frac{1}{4}$,
Section 33: W $\frac{1}{2}$ W $\frac{1}{2}$, SE $\frac{1}{4}$ SW $\frac{1}{4}$, S $\frac{1}{2}$ SE $\frac{1}{4}$,
Section 34: S $\frac{1}{2}$ SW $\frac{1}{4}$, W $\frac{1}{2}$ SW $\frac{1}{4}$ SE $\frac{1}{4}$.

Furthermore, Utah Highway 53, a public road, passes through the proposed buffer zone. A legal description of the specific surface area containing the public road is as follows:

Township 12 South, Range 12 East, SLB&M:

Section 28: SW $\frac{1}{4}$ SW $\frac{1}{4}$, Section 33: W $\frac{1}{2}$ NW $\frac{1}{4}$.

A copy of the current mine permit and the application for a significant revision is available for public inspection at the Carbon County Clerk's Office, Price, Utah, and the Utah Division of Oil, Gas and Mining. Any comments should be directed to the Utah Division of Oil, Gas and Mining, 355 West North Temple, 3 Triad Center, Suite 350, Salt Lake City, Utah 84180-1203.

Published in the Sun Advocate _____, 1992.

The proposed plan consists of a single mine located in the Rock Canyon seam and accessing coal reserves in the overlying Sunnyside seam and underlying Gilson seam via underground rock slopes. The methods of coal removal will be the same for each horizon worked within the mine. The exact method for any given area of the mine will vary, depending upon surface and subsurface sensitivities, depth of overburden and multiple seam conditions. The two basic methods to be used are longwall and room and pillar mining. A detailed description of methods to be used are given in Section 5.22 and 5.23.

Room and pillar mining will be used to develop main, submain, and panel entries. In addition, this method will be used in areas which are uneconomical for longwall mining due to reserve geometry. Also room and pillar mining using limited extraction will be used in areas where high to total extraction methods are inconsistent with our subsidence control plan. Longwall mining will be used to achieve maximum extraction in those areas where it can be economically applied in harmony with the subsidence control plan.

As a result of the Applicant's proposed mining activities, some subsidence is expected to occur above much of the full extraction longwall areas. Exhibit 5.25-1 shows the areas over which maximum subsidence may result from the proposed mining activities.

The Mine Layout Design and Ventilation Analysis prepared by J.F.T. Agapito & Associates, Inc. (Appendix 5-D) also evaluated the potential surface subsidence of the proposed mine plan. Utilizing a modified National Coal Board method, which is based on measurements from western U.S. mines, it was estimated that the maximum total subsidence would be approximately 12 feet for 2 seam full extraction. A subsidence factor of 70 percent and an angle of draw of 22.5 degrees was used for the above evaluation. (The subsidence factor is the ratio of maximum surface subsidence to total mining height and the angle of draw defines the expected limits of surface subsidence beyond the boundaries of full extraction.)

5.25.12 Description of Physical Conditions

The depth of cover, seam thickness and lithology, which affect the likelihood or extent of subsidence and subsidence related damage are shown on the mine progress, interval, isopach and subsidence maps and addressed within this section and in the mine planning section.

5.25.13 Measures to Prevent Subsidence

In areas where mining may cause undesirable surface movement, steps will be taken to control or prevent subsidence. To prevent subsidence, permanent support can be achieved by selectively mining certain areas, leaving support pillars of coal, and/or by not mining specific areas.

The proposed mine plan identifies a zone of no secondary mining (Exhibit 5.25-1). This zone is designed to protect Soldier Creek, the Western Natural Gas, Inc./REI degasification facilities, the public road and a portion of the existing Questar natural gas pipeline. The route of this pipeline leaves the zone of no secondary mining as it turns east into Pine Canyon and continues northeast over the mine plan area. Since full extraction longwall mining is proposed for this area, alternative methods of pipeline protection must be evaluated. Agapito & Associates (1991), suggest that uncovering the pipeline through this area may adequately protect it from subsidence damage. Also, the Applicant is presently in discussion with Questar Pipeline Company regarding the possible relocation of their gas pipeline around the proposed full extraction areas. Questar's preliminary reroute proposal is presented in Appendix 10 as Illustration 10.5.25-1. In any case, an agreement between Questar Pipeline Company and the Applicant shall be executed, and incorporated into this MRP, prior to the commencement of any full extraction mining beneath the existing pipeline.

Agapito & Associates, 1991 (Appendix 5-D) specifically analyzed the potential mining impact to Pine Creek at the point of minimal overburden (approximately 1370 feet). Their analysis is as follows:

USBM (Babcock and Hooker, 1977) suggest several criteria for full extraction

mining under major water bodies. These are:

- * The cumulative, calculated tensile strain beneath a body of surface water of major potential size shall nowhere exceed 15×10^{-3} . This criteria is satisfied for Pine Creek as the maximum calculated strain is 11.2×10^{-3} , near the intersection of the Pine Creek and the longwall barrier pillars.
- * Where more than one seam exists, all may be worked by total extraction provided that there is a minimum overburden thickness equal to 58 times the total thickness of all seams to be extracted. This criteria is also satisfied as the minimum overburden thickness is approximately 1350 feet.
- * Where a fault which might connect mine workings with the surface stream having a vertical displacement greater than 10 ft is known to exist, no seam should totally be extracted within 50 ft of the faults. Currently, there is no known major fault in the reserve.

At the time of mine abandonment, the Applicant proposes some limited backfilling of mine entries. These entries are associated with the existing mine ventilation shaft, and lie directly beneath the Soldier Creek channel. All such entries, which have less than 100 feet of overburden shall be backfilled with available underground development waste. Backfilling of additional entries with 100 to 250 feet of overburden may also be considered, but only if these entries show significant signs of deterioration upon abandonment. It should be noted that the available information on pillar strengths and overburden characteristics indicate that backfilling is not required for long-term stability. The backfilling proposed is considered a precautionary measure only.

5.25.14 Monitoring

Subsidence monitoring will be carried out on an annual basis and will entail direct surveys and visual surveys of the mine permit area. The major concern of the subsidence monitoring will be the renewable resources, perennial streams, perennial springs and gas line within the permit area. The methods to be used for monitoring will be ground surveys of monuments and visual surveys during

water monitoring or any other surface activities. Initial subsidence monitoring began in 1987 and will continue throughout the life of mine. Annual reports will be sent to the Regulatory Authority detailing all subsidence monitoring activities. The 1987 through 1991 subsidence monitoring summary sheets are presented as Tables 5.25-2 through 5.25-6 respectively. Subsidence data is also located in the annual reports and Table 5.25-7. Also the monuments which have been monitored through 1990 are shown on Exhibit 5.22-1 & 5.25-1.

Monitoring will entail the establishment of surface control monuments within and adjacent to the permit area. This initial survey will provide the Applicant with a base network which will be expanded each progressive year to obtain subsidence information over the permit area. The expanded network will cover the expected development for each progressive year. Each monument will have horizontal and vertical control determined during the initial survey. This information will be used as a comparison tool for all future monitoring.

Annual resurveys of the mine permit area will produce vertical control at the same sites as the previous year (i.e. the base network and all expanded networks). Information on each site will continue to be produced annually while the area underlying the site is being actively mined or is still unstable and subsiding. The subsiding areas which show no change for two consecutive years will be considered stable and will be omitted from further annual surveys. The annual subsidence survey was discontinued with the survey performed in the year 2000. No tangible surface change was noted in the surveys performed in the years following the cessation of mining as noted on Table 5.25-7. Additional survey data can be found on Tables 5.25-2 through 5.25-6 and in the annual reports.

If mining within the dropped sites happens to occur, then the sites will, again, be added to the annual surveys. Also, during random years, some of the dropped sites will be monitored as a check on their stability and any showing a significant change will be included in the following year's monitoring.

In addition to the ground surveys, aerial photogrammetric methods will be included in the surveys when the areas become too large to feasibly handle with ground surveys. This method will be added to enhance the ground surveys and to

cover larger areas as our mine expands to the boundaries. Visual checks for subsidence will be made during all surface activities, especially during water monitoring activities. These visual surveys will be used to detect surface irregularities, surface cracks, and as a check on the direct surveys or any future aerial surveys. Each year a subsidence monitoring report will be sent to the Regulatory Agency. The report will include; dates of surveys, methodology used, results obtained, and mitigative action taken to correct subsidence caused effects. This report will also include changes in the monitoring plan that may be made owing to economic conditions or technical advancement in the art of subsidence monitoring.

	1998	Difference	1999	Difference
	Elevation	1997 -	Elevation	1998 -
-0.57	7755.06	-0.08	7755.10	0.04
-0.29	7816.64	0.23	7816.42	-0.22
-1.54	7732.41	-0.26	7732.68	0.27

Point #	Original Elevation	1997 Elevation	Orig. - 1997									
113-SS	7755.71		7755.14									
92-1SS	7816.70		7816.41									
93-1SS	7734.21		7732.67									

113-SS established 1980

92-1SS established 1992

93-1SS established 1993

5.25.16 Mitigation of Damages

While no damage is anticipated as a result of subsidence from the proposed mining operations, should material damage occur in spite of prevention measures, the Applicant will repair the damage and comply with R645-301-525.230. The Applicant will notify the Regulatory Agency of any slide, rock fall or other disturbance that will have an adverse affect on the environment. If the existing gas pipeline is damaged as a result of subsidence, the pipeline will be repaired by the Applicant. If the roads mentioned earlier are damaged by subsidence, the Applicant will restore the roads to their pre-subsidence usefulness.

5.25.20 Subsidence Control

Soldier Creek Coal Company (SC3) will comply with all provisions of the approved subsidence control plan. SC3 will correct any material damage resulting from subsidence to surface lands, to the extent technologically and economically feasible, by restoring the land to a condition capable of maintaining the value and reasonably foreseeable uses which it was capable of supporting before subsidence.

Material damage resulting from subsidence caused to any structures or facilities will be corrected by repairing the damage or compensate the owner of such structures or facilities in the full amount of the diminution in value resulting from the subsidence.

The proposed mine plan will not operate under or in close proximity to any urbanized areas or public buildings.

Also, the mine plan is designed so that mining will not result in material damage to perennial streams or impoundments having a storage volume of 20 ac-ft or, which could result in environmental degradation or safety hazards to streams, water bodies and associated structures. Furthermore, the proposed mine plan is compatible with conservation of existing aquifers within the permit area.

5.25.30 Public Notice of Proposed Mining

Each owner of property or resident within the area above an underground mining block and adjacent area that could be theoretically affected by subsidence, even though it may not actually occur, will be notified by mail at least six months prior to mining or within that period if approved by the Division. The notification shall contain:

- a. Identification of specific areas in which mining will take place.
- b. Dates of underground operations that could cause subsidence and specific structures; and
- c. Measure to be taken to prevent or control adverse surface effect.

5.25 Refuse Disposal Site

~~Since no underground mining activity has occurred or will occur beneath or in the immediate area of the previously proposed site, no subsidence is anticipated at the site. Due to settlement of the refuse and elastic compression of the underlying bedrock, it is expected that settlements on the order of 0.5 to 1.0 inches will occur following completion of the disposal area. Some differential settlement of the fill and redistributed topsoil and cover materials will also occur. This minimal settlement is not expected to result in any significant impacts to the site or reclaimed surface.~~

5.26 Mine Facilities

Central Mine Facilities

Soldier Creek Coal Company's (SC3) new surface facilities expansion and road relocation will provide the needed facilities and space to accommodate an increase in coal production and preparation for up to 3.5 million tons/year.

Surface buildings and structures that presently exist (Table 5.26-1) and those described, immediately following Table 5.26-1, will be used in connection with or to facilitate the underground coal mining activities at the Soldier Canyon Mine (SCM), located 12 miles north of Wellington, Utah. The existing and proposed facilities are shown on Exhibit 5.21-1. Construction on all proposed

facilities shown in this section (5.26) will begin by September 15, 1996, and will be completed within a two year construction time frame. Any facilities not started by this date will either be deleted from the permit or the permit will be changed to show a new construction starting date.

As depicted on Exhibit 5.21-1, the surface facilities do encroach upon the county road and Soldier Creek. In order to minimize the impact on the water quality, degradation of stream channel and facilitate the road relocation, the applicant installed approximately 885 feet of culvert. The stream culvert was installed following DOGM's approval of two previously submitted permit amendments (Illustration 10.2.2-1 and 10.2.2-2). The road relocation has been approved by the BLM and Carbon County. Approval to relocate the county road was granted by the Division on July 19, 1991.

All of the facilities presently constructed and to be constructed will be designed for the LOM. The Applicant plans to use all facilities for the normal operation of SCM and will repair or replace the facilities with items of similar performance standards throughout the LOM. The facilities expansion structures will be constructed and meet the performance standards to provide adequate compliance so that no significant harm to the environment, public health or safety will result from the use of the structures.

Measures have been taken by SC3 to ensure the protection of the landowner and public. The BLM (landowner) reviewed the road relocation project and has issued the Applicant the necessary right-of-way permit (Illustration 10.2.1-1). Carbon County has also reviewed the road relocation project and has given their approval (Illustrations 10.2.1-2 and 10.2.1-3).

The facilities and yard expansion will be fenced for security purposes and access to the facilities will be controlled by roadside gates (Exhibit 5.21-1). The fence will be a type A galvanized wire fence, will stand 7 ft. high and supported by 8.5 ft. galvanized steel posts spaced 9 to 10 ft. apart. Fence construction is in accordance with BLM's Land Management Handbook and has barbed wire suspended from the top.

The conveyor structure leaving the ROM transfer house will cross the county road totally enclosed, via a tube, and have a 58 foot clearance between it and the county road (Figure 5.26-1).

The construction of the surface facilities expansion will allow the Applicant the ability to continue their operation of SCM and improve the coal handling facilities. The initial construction drawings and plans are shown on Exhibits 5.21-1 and Exhibit 7.32-1. During the construction of the facilities, modifications to the drawings and plans may occur, but all modifications will be shown on the final as-built drawings sent to DOGM. Any modification that could alter or effect the design of the runoff controls or the stream culvert will be sent to the state prior to construction of the facilities.

Designs of the surface facilities expansions at SCM is based on present coal handling problems, ventilation requirements and long-term needs for both at SCM. The following facilities will be constructed during 1992/1993, except for the Portals that were started in October 1989 and completed in August 1991.

1. Three Portals into the Rock Canyon seam will provide additional intake air capacity and will allow SCM to change their underground conveyor facilities.
2. Fourth North #1 belt will connect the underground conveyor system to the surface facilities. This belt has been designed to carry coal from the mine at 3600 tons per hour. The belt will be covered for the total length that it is exposed on the surface.
3. The Transfer House with Crusher will be enclosed and equipped with water sprays. Coal will be transferred from the Fourth North #1 belt, crushed to 5"x 0 and then onto the silo conveyor belt.
4. Silo conveyor belt will accept coal from the Fourth North #1 belt and has been designed to handle 3600 tons per hour. This belt will be covered for the entire length. This belt will discharge coal into the silos. It will have a dribble pan/tube where the belt crosses the county road. The

transfer points from the belt to the silos will be enclosed and equipped with water sprays.

5. The silos will accept coal from the silo conveyor belt. One silo will be equipped with an overflow chute to provide for emergency ground storage.
6. Vibrating feeders will be placed within the silos and ground storage facility to draw coal from the facilities and dump the coal onto the reclaim belt.
7. A Reclaim Tunnel will be placed beneath the silo pads. The vibrating feeders will be anchored to the tunnel and a reclaim belt will be placed within and anchored to the tunnel.
8. The Reclaim Conveyor Belt will accept coal from the vibrating feeders and convey the coal to the Preparation plant. This belt will be covered for the total length that it is outside the reclaim tunnel.
9. The Baum Jim Preparation Plant will be enclosed and house the equipment necessary for washing coal as needed. Two crushers will be enclosed within the preparation plant. Due to the location of the crushers, water sprays are not anticipated. One crusher will be used to size coal to 2"x0 when coal quality is such that washing is not necessary and the system is by-passed. The other crusher will be used for the cleaned coal at the end of the washing cycle. Processed coal will then be transferred to the truck bin belt. Refuse from the washing process will be transferred to the refuse bin conveyor.
10. An Ash Analyzer, used in monitoring coal quality, will be located along the coal conveyor belt at the coal bins.
11. The Truck Bin Conveyor Belt will accept coal from the preparation plant and will convey and discharge coal to the truck bins. The transfer point from the belt to the truck bins will be enclosed and equipped with water sprays.

12. Two 600 ton Truck Bins will accept the coal from the truck bin belt and discharge the coal into coal haulage trucks. The bins will be equipped with sensors that will automatically open and close the dump gates of the bins.
13. The Refuse Conveyor Belt will accept refuse from the preparation plant and will convey and discharge refuse to the truck bin. The transfer point from the belt to the truck bin will be enclosed, but not equipped with water sprays.
14. The 300 ton Truck Bin will accept the refuse from the refuse conveyor belt and discharge the refuse into refuse haulage trucks. ~~Refuse will be hauled to the waste rock disposal site.~~
15. Thickener Tank is used in the recovery of coal fines from the washing process. These fines settle out through the use of polymers and are then sent to a filtering disc where the caked fines are discharged onto the truck bin conveyor and blended with the coal.
16. Power Poles will be repositioned and several new poles added to provide electrical power to the facilities.
17. Substation 46 KV will be constructed to supplement the present power source needed to operate the new facilities.
18. A culvert has to be placed into the natural channel of Soldier Creek to allow for the construction of the facilities and to protect this water resource. The culvert was designed for the 100-year, 24-hour storm event.
19. County Road will be relocated eastward to facilitate SCM's expansion. The new road will be built using current and prudent engineering practices. The road will be a county road and maintained by the County.
20. Access Roads into the expansion will provide an access to the mine portal area and haulage facilities. These access roads will be classified as

primary roads and constructed to meet all prudent regulations.

21. A Concrete Protection Pad has been placed over the gas line to permit haulage of men and material over the gas line and into the portal area.
22. Drainage controls will be placed within the expansion to provide runoff control for the surface facilities, yard expansion, and undisturbed drainage. Additionally, several operational drainage controls may be upgraded to provide the necessary facilities to handle the design event.
23. Fences and Gates will be placed along the county road and across the culvert in the stream to limit any unauthorized access to the surface facilities expansion. Also, the fence enclosing the present storage yard will be removed and relocated to accommodate the new facilities.
24. Other miscellaneous items may be added to the design to improve the overall operation of the facilities, but all such items will be listed and shown on the as-built drawing that will be submitted to DOGM.

Topsoil Storage Site

The Topsoil storage site was constructed to handle the storage needs of the mine. The site is located approximately 2.5 miles southwest of the mine and is located within 100 feet of a public road (Exhibit 5.21-2).

The storage site is 4.5 acres, of which only 2.3 acres is presently being used for the storage of topsoil, substitute topsoil and landscape boulders/riprap. ~~Upon approval of the refuse disposal site, the remaining acreage will be used for the storage of topsoil and subsoil that will be harvested prior to placement of refuse.~~

Refuse Disposal Site

Previous submittals have included sections on a refuse disposal site. These references have been omitted from this chapter since this site is no longer proposed for the Soldier Creek Mining operation. The operational history has

shown little need for such a site. Disposal, if any should occur, will be either at the Skyline or SUFCo disposal areas.

~~The refuse disposal site is located approximately 3.0 miles southwest of the mine site. The construction of the site is necessary for disposal of coal mine waste that will be generated during operation of the preparation plant and other underground operations.~~

~~No buildings or utilities are planned for the operation of the refuse disposal area. Facilities will include the access road, the refuse disposal area, diversion ditches for the disturbed and undisturbed areas, and a sediment pond. The access road is discussed in sections 5.27 and 5.34 of this application. The refuse pile is addressed in sections 5.28 and 5.36 of this application. The diversion ditches and sediment pond are discussed in sections 5.32, 5.33 and Chapter 7.0 of this application.~~

5.26.20 Utility Installations and Support Facilities

5.26.21 Utility Installations

Questar Pipeline

A Questar Pipeline Company gas line passes through the property in a northeasterly direction. The pipeline was constructed in 1962-1963 and is presently in use (Exhibit 1.12-1).

Methane Recovery Facilities

Resource Enterprises, Inc.'s (REI) methane collection facility offices and storage yard are located within the mine permit boundary. These facilities include gas collection and pump systems, office, bathhouse and storage yard (Exhibit 5.21-1). REI's methane gas recovery operation exploits the coalbed gas resource by working in unison with the underground mining operation. This operation holds permits and approval from the Mine Safety and Health Administration and the BLM. The produced gas is sold to Questar Pipeline Company and injected into their pipeline which passes through the Applicant's permit area.

Power Supply

Utah Power provides electrical power for the entire mining operation. Presently, two substations distribute power to the underground equipment and surface facilities with a third substation, planned for construction during the facilities expansion (Exhibit 5.21-1). The existing substations and the planned substation, are and will be 46 KV. The electrical system complies with all federal, state and local requirements. The transmission lines were constructed by Utah Power & Light and Electrical Contractors and have raptor-resistant towers to minimize the potential for adverse impacts to wildlife (Figure 5.26-3).

Disturbance caused by company own transmission lines is very minimal. Transmission poles are spaced approximately every 200' - 400'. Disturbance at each site is usually limited to a 2' diameter area. Using Soil Conservation Service formulas:

$$Q = \frac{(P - 0.5S)^2}{P + 0.8S}$$

$$S = \frac{1000}{CN} - 10$$

S = Watershed storage factor (inches)

P = Rainfall depth (inches) = 1.90" 10 year-24 hour event

CN = Runoff curve number (dimensionless) = 75

Q = Direct runoff volume (inches) = .333" calculated

The total runoff from each site is .65 gallons. This runoff is very minimal and due to vegetative cover and low flow velocities, erosion is not a problem. If erosion should become a problem, sediment control structures such as straw bales and silt fences could be used. Refer to Figure 5.32-1 page 5-50a for sediment control structures.

Diesel generators provide emergency power to the ventilation fans in the event of a power failure.

Communications

A telephone system tied into the U.S. West Communication's system provides direct communication between the portal area in Soldier Canyon and the central facilities area. A sufficient number of hook-ups have been installed to provide easy access in case of an emergency.

In addition, an independent, private system is functioning. This system includes hook-ups in the mine to provide communication with the portal and central facilities areas. It was designed for easy and rapid access to maximize safety and complies with all current MSHA requirements.

The Applicant's coal mining and reclamation activities will be conducted in a manner which minimizes damage, destruction, or disruption of services provided by gas, electric and telephone lines which pass over, under or through the permit area, unless otherwise approved by the owner of those facilities and the Division.

5.26.22 Support Facilities

All support facilities incident to the operation of Soldier Canyon Mine will operate in accordance with a permit issued for the mine. Support facilities will be located, maintained, and used in a manner that prevents or controls erosion and siltation, water pollution, and damage to public or private property; and to the extent possible using the best technology currently available minimizes additional damage to fish, wildlife and related environmental values; and minimizes additional contributions of suspended solids to stream flow or runoff outside the permit area. Any such contributions will not be in excess of limitations of Utah or Federal law through adequate design and operation of appropriate water pollution control facilities.

A step-by-step progression through the coal conveyance facilities, potential waste material and water discharges is shown on Figure 5.26-1 and 5.26-2.

1.0 Liquid discharges from the facility during normal operations and maintenance operations are discussed below.

1.1 Washdown Effluent from the Covered Portion of the #1 Raw Coal Transfer Conveyor

This will be routine maintenance operation to take care of any coal spillage that remains after the material has been shovel cleaned. The effluent will be collected in a catch pan fitted with a ½" aperture screen. +1/2" material will be shovel cleaned off the screen. Material and water passing through the screen will be directed to the yard drainage collection ditch below. Hose output would be 35 to 50 gallons per minute.

1.2 Washdown Effluent from the Silo Reclaim Area Including the Conveyor Extension

This will be a routine maintenance operation for coal spillage in the area that remains after shovel cleaning. The hose water and coal will be washed down to a collection sump at the rate of 35 to 50 gallons per minute. The collection sump will be fitted with a ½" aperture screen. Plus ½" material will be shovel cleaned off the screen. Material and water passing through the screen will be pumped via units (111A) and (111B) into the yard drainage collection ditch adjacent to the silo. Each pump is capable of 75 gallons per minute and only one pump should be operated at one time. Pump start-up and shut-down is controlled by high and low level float controls.

Any silo pad drainage water that may pass through the reclaim hopper together with any water drainage from the silo contents will also eventually end up in the collection sumps.

1.3 Effluents from the Coal Preparation Plant

There should be no discharges from the plant during normal operations as it uses a closed loop concept.

During coal washing operations the plant requires an addition of water to make-up for the losses contained in the moisture added to the refuse and cleaned coal product. These losses are in the order of 19 gallons per minute.

All water used inside the plant is reclaimed and recycled. Washdown water used both during washing hours and non-washing hours is also reclaimed.

Unless there is a simultaneous failure of both clean-up sump pumps in the plant, all liquids contained within the plant that pass onto the ground floor will pass to either the fine coal (jig) sump or in an emergency situation to the sediment pond via the yard area ditch. Mr. Michael D. Herkimer, Division of Water Quality (DWQ), told Tom Paluso on August 13, 1992, that Soldier Creek would be allowed to discharge to the sediment pond during emergencies. DWQ would have to be notified of these discharges.

A copy of our present NPDES permit is on page 5-39b, Illustration 5.26-1.

In the event that a surplus of water exists in the plant due to operator error, the floor clean-up sumps are fitted with manually operated, valve by-pass pipes delivering the water to the sediment pond via the drainage ditch.

1.4 Drainage from Loadout Bins

Depending upon the length of time that the material is stored in the specification coal and refuse bins, there may be some drain down of the surface moisture.

This water will pass via the yard area into the drainage ditches. ~~Extra dewatering capacity has been included in the preparation plant in the refuse circuit to minimize this problem.~~

2.0 Liquid Discharges from the Facility During Maintenance Operations

Other than the preparation plant, there should be no additional liquid discharges from the rest of the facilities that are not described in Section 1.0.

2.1 Preparation Plant

Most maintenance situations can be handled without any outside discharges of

liquids.

There are, however, three major liquid storage vessels forming part of the preparation plant that may affect this:

1. The fine coal (jig) sump which contains approximately 43,000 gallons maximum
2. The clarified water sump containing 9,300 gallons.
3. The thickener containing approximately 90,000 gallons.

The thickener and the fine coal sump contain a mixture of water and fine coal (minus 100 mesh and 0.75 mm respectively) during normal washing operations.

The fine coal sump is fitted with high and low level drain connections, discharging to the floor. In the event that too much water was allowed to accumulate in that circuit due to operator error, the high level drain could be utilized to drain off excess liquid. If this was done during operations, the liquid would contain fine coal. During shut down periods the liquid would be "clear". The drainage would pass via the floor collection sump pump to either the fine coal sump for solids recovery or directly to the sediment pond via ditch if the liquid was "clear". The above scenario would also apply if ever the entire sump had to be drained in which case every effort would be made to recover the solids portion of the contents via the cyclone and disc filter circuit.

It should be noted that during normal operations, the jig itself retains approximately 27,000 gallons of the sump contents. This amount will always remain in the jig unless it is physically drained.

The jig would require draining to perform certain maintenance operations. The water would pass into the fine coal sump and any overflow of the sump would be dealt with as described earlier.

The clarified water sump is fitting with a low level drain that discharges onto the floor. The water would then pass into the floor collection sump pump for disposal to either the fine coal sump or sediment pond as described earlier.

The thickener is fitted with a variety of devices to ensure efficient operation and maintenance facilities. It has high and low level drains each piped to the yard area drainage ditch. The thickened sludge from the bottom discharge cone is extracted via dual outlet pipes and pumps (1 operating, 1 standby). Each pipe and pump system is equipped with high pressure water connections for preventative flushing to ensure optimum working conditions after shutdown.

The thickener tank has sludge level sensing device which tells the operator exactly where the separation is between the thickened sludge and clarified water.

For a planned thickener drain down (i.e. with all ancillary equipment working) the thickened sludge would be evacuated via the underflow pumps and recovered via the disc filter. The remaining "clear" water would then be drained via the ditch to the sediment pond. On a sludge worst case basis, approximately half the thickener contents could be sludge, leaving approximately 45,000 gallons of "clear" water to be directed to the pond.

For a worst case unplanned emergency thickener drain down (i.e. no thickener rake rotation availability), the following is one possible procedure.

1. Remove as much sludge as possible via the underflow pumps, disc filter, etc.
2. Drain the fine coal sump (recovering any solids) discharging "clear" liquid to the pond.
3. Use the high level drain on the thickener to discharge the "clear" liquid to the pond.
4. Bring in the external sludge pump and transfer material to the fine coal sump.
5. Repair/re-instate thickener
6. Pump transfer fine coal sump sludge back to thickener.

As stated in Section 7.42-3, the Applicant will discharge from the plant only if no precipitation event is occurring, unless operational and safety hazards are imminent.

3.0 Anticipated Oversize and Undersize Waste Material

There is only one size of waste material produced by the preparation plant which is not added to the specification coal conveyor, this is the refuse product. The typical amount is shown on the flowsheet. This will vary depending on the raw coal quality.

Culinary Water

The Applicant purchases all culinary water from D& D Equipment and Supply Distributors of Helper, Utah. D&D purchases culinary water from Price City and Wellington City public water loadouts. Deliveries are made twice a day and total approximately 3,000 gal. The holding tank at the mine site has a capacity of 60,000 gal.

Sanitary Wastewater

Soldier Canyon Mine uses a total containment lagoon system constructed in the fall of 1982 to treat wastewater. The system includes a metal septic tank, a sewer line and 2 self-contained lagoons having a surface area of 0.14 ac each (Exhibit 5.26-2).

The septic tank located at the mine site is coated according to Underwriters Laboratories, Inc. specifications UL 70 and is used to collect all solids before releasing the water into the 4 in. line. The water is then transported to the lagoons, approximately 11,655 linear feet southwest of the main facility area, by the 4 in. gravity flow line. Along the line there are several cleanouts to ensure proper functioning. The water exits the pipeline and empties into the containment lagoons which consist of two clay-lined cells with a designed capacity of over 3,200 gal. of wastewater per day. Each cell is lined with clay to limit seepage to 0.125 in. per day. The embankment slopes are 3:1 and are riprapped.

A contract hauler transports sludge from the septic tank to the Wellington wastewater treatment plant for disposal or to the sewage lagoons. The hauler is qualified to dispose of sludge.

The wastewater system was designed by Horrocks and Carollo Engineers with all plans and designs approved by the Utah Division of Health. The location of the lagoon and the pipeline system are shown on Exhibit 5.26-2. The lagoon is surrounded by Type A galvanized wire fencing to keep out deer and other large mammals. Sludge remaining after evaporation will be disposed of on-site or may be used for soil reclamation. Dikes and the area around the lagoons have been successfully revegetated.

Mobile Screening Unit

The Applicant will at times use a mobile screening unit to screen run-of-mine coal at the mine site. The screening unit is proposed to be used occasionally, until the new surface facilities can be constructed. The screener will be placed adjacent to the existing ground storage stockpile and coal will be supplied for screening via a front-end loader. The screened coal will be stockpiled, and the coarser material will be placed back on to the original stockpile and transported to Banning for processing. Exhibit 5.21-1a shows the approximate location of the screener and associated screened coal stockpiles.

5.26.3 Water Pollution Control

Industrial Wastewater

Any ground water which is encountered is collected in sumps and pumped into Soldier Creek in accordance with 614-301-731 and 614-301-751 and the National Pollutant Discharge Elimination System (NPDES), Permit No. UT-0023680 (Table 5.26.2). In accordance with R614-301-731.222.2 the Applicant will notify the Regulatory Authority within five days of receipt of analytical results that indicate noncompliance with permit conditions. At least every three months monitoring data will be submitted to the Division.

Wastewater produced from mine equipment washdown or facilities cleanup vary widely in volume and concentration of wastes. These wastes are treated in grease and sediment traps at the sources and either recycled or discharged to the sediment pond.

5.26.4 Air Pollution Control

Coal mining and reclamation activities will be conducted in accordance with R614-301-420 and the Air Quality Approval Order issued by the Utah Division of Air Quality (Appendix 4-D).

5.27 Transportation Facilities-Road Classification

Central Mine

There is one main road leading to Soldier Canyon Mine, Soldier Creek Road. This 30 ft. wide road, maintained by Carbon County, is paved to the mine site. Beyond the mine the road is graveled for several miles, branching in Sec. 32 T12S, R12E with one branch going northeast through Nine Mile Canyon and the other to the northwest. Other portions of the permit area may be reached by sporadically maintained trails and jeep trails. Mine staff infrequently use (4 time per year) ranch roads to access water monitoring locations (Exhibit 7.21-1).

The No. 1 exhaust fan, two ventilation slopes, water tank, and access road are located directly northwest of the main mine buildings (Exhibit 5.21-1). These facilities were constructed in 1975-76 as part of a major improvement and rehabilitation project of the existing mine. Specific details of the area are shown in Figure 5.27-1.

Design and construction of the No. 1 exhaust fan and associated road preceded the regulations pertaining to surface effects of underground coal mining (i.e., Utah Code Annotated U.C.A. 40-10-1 et seq). The access road, as constructed, does not fully comply with these regulations (specifically R614-301-527.100 and R614-301-534 Primary Roads) However, the Applicant believes for the following reasons, that the existing road meets or exceeds the performance standards intended by complying with R614-301-527.100 and R614-301-534.

1. All runoff from the road is conveyed directly to the central facilities sedimentation pond. This sedimentation pond provides the best available runoff treatment to prevent additional contributions of suspended solids to the natural drainage.

Table 5.26-2

NPDES Effluent Limitations
(Permit No. UT 0023680)

During the period beginning immediately (July 1, 1991) and lasting through March 31, 1996, the permittee is authorized to discharge from Outfalls 001, 002, 003 and 004. During the permit period, discharge from Outfalls 005, 006 and 007 is only authorized upon completion of a final construction inspection by Utah Bureau of Water Pollution Control and authorized by the Bureau to place the facilities in operation. Such discharges shall be limited and monitored by the permittee as specified below:

<u>Effluent Characteristics</u>	<u>Monthly Average</u>	<u>7-Day Average</u>	<u>Daily Maximum</u>	<u>Sample Type a/</u>	<u>Frequency</u>
Flow, M ³ /day, gpd	N/A	N/A	N/A	2/month	Measured <u>b/</u>
Total Suspended Solids, mg/L	25	35	70	2/month	Grab
Iron (Total), mg/L	N/A	N/A	2.0	1/month	Grab
Total Dissolved Solids, mg/L <u>c/</u>	N/A	N/A	1,200	2/month	Grab
Oil and Grease, mg/L	N/A	N/A	10	1/month	Grab

The pH shall not be less than 6.5 standard units nor greater than 9.0 standard units and shall be monitored twice per month by grab sample.

There shall be no discharge of floating solids or visible foam in other than trace amounts.

Samples taken for compliance with the monitoring requirements specified above shall be taken at the discharge points prior to mixing with the water in Soldier Creek.

a/ See Definitions, Part I.A.

b/ For the intermittent discharges, the duration of the discharge shall be reported.

c/ In addition to the concentration limitation, the total amount of Total Dissolved Solids (TDS) discharged

from all outfalls is limited to five tons (10,000 pounds) per day.

2. Adequate drainage and erosion controls have been constructed and maintained by the Applicant.
3. The horizontal and vertical alignment of the road has provided acceptable access while minimizing the area disturbed. Alternative alignments were very limited due to the extreme rugged terrain of the area.
4. Road cuts and embankments constructed in 1975-76 have demonstrated adequate stability.
5. Final reclamation for the site has been addressed and approved.

The surface expansion will involve the relocation of the county road and the establishment of two primary roads. The county road will be constructed according to the County and BLM specifications. As shown by the County and BLM approvals, the road satisfies their requirements. Although the County will operate and maintain the new road, the Applicant will maintain reclamation liability for the area throughout the bond liability period.

The two primary roads will be constructed and maintained according to the regulations. The primary road leading into the yard will split in order to access the haulage facilities. The other primary road will access the new portals. Exhibit 5.21-1 and Figure 7.32-1 show the new location of the roads and typical design. As-built drawings and certification of the primary roads will be submitted upon completion of construction of the new operations.

Sewage Lagoons

Accessing the sewage lagoon is an ancillary road, approximately 1,000 ft. in length extending from the Soldier Creek Road to the sewage lagoon (Exhibit 5.26-1). Mine staff infrequently use this (4 times per year) to inspect the lagoon and diversion structures.

Topsoil Storage Site

Accessing the topsoil storage site is a ancillary road, approximately 100 ft. in length extending from the Soldier Creek Road to the storage site (Exhibit 6.1-1). The road will only be used when material is to be stockpiled and for monitoring

diversion structures and vegetation. The designs, specifications, and plans for this road are presented or discussed in section 5.34 of this application.

Refuse Disposal Site

~~The refuse material will be transported from the mine site to the disposal site via the county road. The access road to the refuse disposal area is located approximately 3 miles from the mine site. The trucks conveying refuse to the site will not be overloaded, therefore, spillage and wind losses should not occur in route. If any spillage does occur, it will be cleaned up and transported to the disposal site as soon as practical.~~

~~The access road will be classified as a primary road and will be used for the purpose of hauling refuse to the site for disposal and water for dust suppression. The road will consist of a paved all weather surface from the county road to the crest of the ephemeral drainage (See Plate 5-1). The road into the drainage will consist of a graveled surface which will be treated to minimize dust and maintenance. Life of this road will be for the life of the facility, following which the road will be reclaimed. The location of the all weather section of the road will not change during the life of the road, while the gravel portion will have a dynamic location depending on the location of the active refuse disposal area. The designs, specifications, and plans for these roads are presented or discussed in Section 5.34 of this application.~~

~~A secondary road, for access to the sediment pond and water monitoring wells, will be located and constructed in the bottom of the drainage from the head of the drainage to the sediment pond location. The road will consist of a graveled surface which will be treated to minimize dust and maintenance. The life of this road will also be for the life of the facility, however, due to incremental enlargement of the refuse pile, the length of the road will decrease as the pile size increases. The designs, specifications, and plans for this road are presented or discussed in Section 5.34 of this application.~~

5.27.2 Transportation Facilities

The present coal haulage conveyor used in carrying coal from the underground

workings to the surface facilities is a 42 in. wide conveyor belt. The conveyor extends beyond the portal to the coal loadout bin. The belt conveyor, constructed in 1976, has a rated capacity of 1,000 tons/hr.

On the surface, the coal is conveyed to and stored in a 600 ton surge bin with automatic truck loading equipment capable of loading 250 tons/hr. Constructed during June and July 1977, the 600 ton capacity loadout bin provides sufficient storage to accommodate production fluctuations.

The coal is then trucked (42 ton/load) by a contract hauler down the canyon 19.3 miles to the Banning Siding Loadout facility operated by Coal Service Company. The Applicant performs no additional processing or preparation on the coal before shipment. However, Coal Service does maintain a crusher at the train loadout facility which reduces the product to 2x0 in.

As shown on Exhibit 5.21-1, the coal haulage, storage, preparation and loadout facilities will be improved to accommodate any projected increase in coal production up to 3.5 million tons per year. The flow sheet (Figure 5.26-2), shows the flow of coal exiting the mine, via the 4th North conveyor, and the step-by-step progression through the coal conveyance system. Exhibit 5.26-1 shows the conveyor profiles to be constructed, used and maintained upon completion of the new surface facilities.

Two ground storage stockpiling locations will be used in connection with the facility expansion (Exhibit 5.21-1). One, is located adjacent to the coal silos and will occur as a result of overspillage from #2 coal silo. The other ground storage is adjacent to the existing loadout bin and present coal stockpiling area. The coal stockpiling capacities will be approximately 3000 tons and 10,000 tons respectively.

When the new facilities are operational, the present conveyor structure will no longer be used and eventually removed. The portion of the existing conveyor that conveys coal to the loadout bin will remain and may eventually be used to provide the operation with the facility to stockpile the approximate 10,000 tons of coal

ground storage adjacent to the loadout bins.

5.28 Handling and Disposal of Coal, Overburden, Excess Spoil and Coal Mine Waste

During the construction of the facilities and further development of the new portals, excavated and underground development material will be generated. The Applicant will temporarily store this material on site (Exhibit 5.21-1a) until the material can be utilized in the construction of pads and roads for the facilities. ~~Any excess material will be removed from the central facilities and placed at refuse disposal site for final placement.~~ During the backfilling of the culvert extension, underground development material was placed at least 8 feet up from the bottom of the culvert to minimize any chance of saturation. The material was analyzed (Illustration 10.2.6-1) and approved by the Division for use as backfill. This will be used for backfilling of the highwalls during reclamation. All underground development materials used in backfilling and grading operations during construction of the new facilities will be accounted for in the reclamation plan and will be placed at the bottom of the highwalls and covered with at least 4 feet of nontoxic and noncombustible material.

~~Until the Applicant's refuse disposal site is constructed,~~ The temporary stockpiling of underground development waste and/or excess spoil will be placed as shown on Exhibit 5.21-1a. Presently, the only anticipated underground development waste will be generated during the grading of the portal roadways. Therefore, a maximum of 1000 yd³ of underground development waste and/or excess spoil will be stored on the operations pad. ~~Upon approval of the refuse disposal site, all excess material will be transported to the site for final placement.~~

Sampling of all future coal mine waste and excess spoil temporarily stockpiled ~~for longer than 3 months~~ will be, by a composite sample and, analyzed according to Table 6 of the "Utah Guidelines for Management of Topsoil and Overburden". ~~Additional sampling will be performed on material placed since the previous sample.~~ Lab results will be submitted to DOGM with the annual report. In the event that acid and toxic forming materials are identified, the Division will be notified and additional sampling of the material will be performed to define the

extent of the problem material.

The sampling program and runoff control, developed by the Applicant, will minimize the potential for any adverse impact to the environment as required by R614-301-731.300.

Overburden material that will be used for pad and other construction at the mine site were sampled for possible toxic contaminants. Representative samples of the overburden and underburden were taken from a previously completed portal exploration cut. Initial samples were taken on 5/8/89 with subsequent resampling completed on 9/30/89. Respective analysis sheets are presented as Illustration 10.2.6-2. (Note: the second analysis was requested by DOGM due to unusually low values originally determined for neutralization are acid potential. Additional detail on % sulfur and % calcium carbonate were also requested).

Based on the 9/30/89 sample analysis, the following values have been determined.

<u>Parameter</u>	<u>Overburden</u>	<u>Underburden</u>
Total Sulfur as S, %	0.03	0.10
Calcium Carbonate as CaCO ₃ , %	20.3	18.8
Acid Potential*	0.94	3.12
Neutralization Potential*	203.00	188.00
Acid Base Potential*	202.06	184.88

*Reported as Tons CaCO₃/1000 Tons Material

Refuse Disposal Site

~~Only a small area of the refuse pile is anticipated to be active at any one point in time. To minimize the area exposed and the area disturbed, the refuse pile will be constructed in segments. Figure 5-1 shows a typical plan view and cross section of the pile operation. The operation of the refuse disposal facility will consist of the following procedures: development of the area of disposal; refuse placement and pile construction; regrading and covering of filled pile sections; and reclamation of the active segment of the pile.~~

Site Development

~~The development of the initial segment of the refuse disposal area will consist of the construction of the runoff control facilities, stripping of vegetation and~~

~~topsoil from areas to be disturbed during the initial segment, and excavation of the subsoil from these areas. The location of the runoff control facilities are presented in the EarthFax Engineering, Inc. report (see Appendix 7-J). These facilities will be constructed prior to any development activities. The runoff control facilities will consist of undisturbed diversion ditches above the facility, disturbed area collection via the existing natural drainage channel below the active refuse disposal area, and a sediment pond. Design plans for these facilities are presented in Section 5.33 and Chapter 7 of this application.~~

~~Prior to the placement of any refuse for the initial or any subsequent segment of the pile, all vegetative cover shall be removed from the area for refuse placement. After removal of the vegetation from the given segment, the topsoil shall be removed, stockpiled, and properly protected for future reclamation purposes. The topsoil stripping plan is presented in Chapter 2 of the application. The topsoil will be stockpiled at the temporary topsoil stockpile area indicated on Plate 5-1.~~

~~A portion of the sub-soil materials beneath the topsoil will also be removed, stockpiled, and protected. This material will be used as fill to cover the refuse following regrading of a prior segment of the pile. The subsoil stripping plan is also presented in Chapter 2 of this application. This material will also be stockpiled at the temporary stockpile area.~~

Refuse Pile Construction

~~The refuse pile construction and placement of material for each segment of the refuse pile will be constructed in 100 foot wide benches with horizontal lifts not to exceed three feet. The refuse material shall be dumped from haul trucks and reworked by suitable earth moving equipment capable of spreading, compacting, and leveling the lifts. This method will assist in achieving the desired densities and prevent the formation of large voids in the refuse materials. Additional compaction for each lift can be achieved by controlling the routing of the loaded haul trucks to cover the entire surface of a given segment of a lift evenly. All construction slopes of the fill outface should not be steeper than 2h:1v. The final exterior slopes of the fill outface should not be steeper~~

~~than 3H-1V.~~

~~The refuse material generated from the coal preparation plant will consist of sandstone, shale and bony coal. The gradation of this material will range from +3/8 inch to -5 inches. All materials -3/8 inch will be shipped with the coal. Due to the anticipated coarse, open graded nature of the refuse material, most quality control work for the pile will be on a visual basis. Conventional in-lace density tests will not give reliable results under these circumstances.~~

~~Based on preliminary analyses of material similar to that which will be placed in the refuse site, no acid or toxic forming problems are anticipated (copies of the laboratory results are presented in Appendix 6-B). Samples of the refuse will be collected quarterly when the site is receiving material and will be analyzed for acid and toxic forming potential. Should a problem be identified, a mitigation plan will be prepared and submitted to DQGM for approval within 30 days of receipt of the analysis. Once the mitigation plan is approved, all identified potential acid and/or toxic forming materials will be disposed of in accordance with the approved plan.~~

~~Noncoal waste and fines from the preparation plant will not be deposited at the refuse disposal site. Noncoal waste will be handled as indicated in Section 7.47. Fines from the preparation plant will be shipped with the coal. The only spoil anticipated from the mine will be from the cleaning of the facilities area sediment pond and excavated material directly related to the facilities expansion.~~

Regrading and Covering

~~Once the lifts of each segment of the pile reach the proposed top elevation for that segment of the pile, the surface of the refuse will be regraded to conform with the proposed final topographic configuration. This material will then be covered with the fill which has been previously removed and stockpiled from a prior segment of the pile. It is planned that future operations of the facility will allow fill and topsoil stripped from expansion sections to be placed directly on areas which have been regraded and are ready to be covered. This~~

~~will minimize the amount of double handling of the materials. This regrading and covering will be conducted in accordance with the regrading and reclamation plans addressed in Section 5.37 and 5.40 of this application.~~

~~The final segment of the refuse pile will have an outslope of 3h:1v. This slope will facilitate the reseeding of the area.~~

~~Following the regrading and cover placement on the current site segment, the stockpiled topsoil will be spread over the regraded segment and will be treated according to the redistribution plan presented in Chapter 2 of this application. Additionally, the current segment of the site will be reseeded and revegetated according to the plan submitted in Chapter 3 of this application.~~

5.29 Management of Mine Openings

During operation of the Soldier Canyon Mine, access to all mine openings are controlled by the operator during working and nonworking hours. For security reasons, the central mine facilities, except for the parking lot, are fenced and access controlled by gates.

Any mine entry that is temporarily inactive, but has a future useful life, will be protected by barricades or other covering devices, fenced, and posted with signs to prevent access into the entry and to identify the hazardous nature of the opening. These devices will be periodically inspected and maintained in good condition by the Applicant.

Permanent sealing of underground openings is discussed in Section 5.51 of this application.

5.30 Operational Design and Plans

5.31 General

The design for the Soldier Canyon Mine facilities and associated sediment control structures are presented in this section.

5.32 Sediment Control

The design of sediment control structures is presented in chapter 7 of this application. The designs are intended to minimize the disturbance to the hydrologic balance by distributing the smallest practical area and through contemporaneous reclamation ~~to stabilize the regraded and contoured refuse material as soon as practical.~~ These activities will result in a reduction of the runoff and sediment rate and volume expected from the site area.

5.33 Impoundments

Central Mine

The only impoundment at the mine site is the temporary sediment pond used for the purpose of sediment control during the life of mine and reclamation operations. The pond was initially designed by Vaughn Hansen Associates in July 1979 and subsequently modified by EarthFax Engineering, Inc. in March 1991. The design of the pond is presented in Chapter 7 of this application. A geotechnical investigation performed on July 14, 1986 of the sediment pond embankment, based on site specific soils information, has shown that adequate safety factors can be maintained. The EarthFax report indicates that the sediment pond has a minimum safety factor for the inslope and outslope of 2.60 and 1.79 respectively. At the same time random compaction tests averaged 95 percent of the maximum dry density as determined by ASTM D-1557. This information is also presented in Appendix 7.

During the pond construction all vegetative and organic materials were removed and the foundation prepared to resist failure. Slope protection is provided against erosion by the existing stand of vegetation.

Refuse Disposal Site

~~No permanent impoundments are planned for the refuse disposal area. The only impoundment planned is the temporary sediment pond used for the purpose of sediment control during the life of the disposal and reclamation operations. This pond has been designed by EarthFax Engineering, Inc. The sizing and~~

~~hydrologic design of the pond is presented in Chapter 7 of this application. A geotechnical investigation of the proposed sediment pond was conducted by BarthFax Engineering, Inc. and is presented in Appendix 5-A. The BarthFax report indicates that the sediment pond will have a minimum 1.5 static safety factor and a minimum 1.2 seismic safety factor.~~

~~The physical design of the sediment pond requires that the foundation and abutments be cleared of all vegetative and organic matter. The foundation site will be excavated to the design depth. The top 9 inches of the area for embankment construction shall be scarified and recompacted to 90 percent of the maximum dry density as determined by ASTM D1557. Moisture content during compaction should be maintained a +/- 2 percent of the optimum as determined by ASTM D1557.~~

~~The embankment fill material shall be placed in horizontal lifts not to exceed 12 inches in thickness prior to compaction. Embankment materials shall be compacted to 90 percent of the maximum dry density as determined by ASTM D1557. Moisture content during compaction should be maintained a +/- 2 percent of the optimum as determined by ASTM D1557.~~

~~Embankment materials shall be free of organic material. The ML materials identified in test pit TP-1 shall be used in the construction of the embankment. No refuse materials shall be used in the embankment fill.~~

~~During the embankment construction, the CMP pipes for the principle and emergency spillways shall be placed at an average gradient of 2.5 percent through the embankment. Structural fill within 2.0 feet of the CMP pipes shall be hand-compacted to a dry density of at least 90 percent of ASTM D1557 at a moisture content of +/- 2 percent of the optimum. During the placement and compaction of the fill along the CMP pipes, the pipes should be preloaded to prevent them from pushing up and out to alignment. Preloads should be maintained until at least one of the pipe diameter has been placed and compacted. Two anti-seep collars within minimum dimensions of four feet by four feet shall be placed around each of the CMP pipes, at 30 foot spacings along the length of the pipes. The anti-~~

~~seep collars shall have water tight connections to the CMP pipes.~~

~~To prevent erosion, the interior and exterior slopes of the embankment should be vegetated with the temporary seed mix as discussed in Section 3.31 of this application.~~

5.34 Roads

General

The primary roads associated with the Soldier Canyon Mine will be located, in so far as practical, on the most stable available surfaces. The roads will be surfaced with rock, crushed gravel, asphalt or other material approved by the Division as being sufficiently durable for the anticipated volume of traffic and weight and speed of vehicles using the road. They will be routinely maintained to include repairs to the road surface, bladeing, filling potholes and adding replacement gravel or asphalt. It will also include revegetation, brush removal, and minor reconstruction of road segments as necessary. Culverts will be installed that are designed, installed, and maintained to sustain the vertical soil pressure, the passive resistance of the foundation, and the weight of vehicles using the roads. All roads will meet the requirement of R645-301-534.200 and R645-301-742.420.

Central Mine

The surface expansion of the central mine facilities will produce two primary roads. The primary road leading into the yard will split in order to access the haulage facilities. The other primary road will access the new portal area. Exhibit 5.21-1 and Figure 5.34-1 show the location of the roads and typical design. For the interim, until the facilities are constructed, the primary roads will not fit the typical design. During construction activities, it would not be practical to asphalt and install the permanent LOM road surface and half-round diversion ditches. Therefore, the Applicant proposes, for the interim, that a graveled road surface and earthen ditches be constructed.

Drainage from the roads will be collected in road side ditches and conveyed under

the roads via drainage culverts. These ditches and culverts are sized to handle the 10 year 6 hour precipitation event. The designs for these structures are discussed in Chapter 7 of this application. To minimize erosion and sediment from the road outslope, the outslopes of the road will be vegetated.

The area not designated as a primary road will be the pad area. The pad areas will be used for mine related storage and activities. Due to the storage of mine related material, the travel paths in these areas will be ever changing in response to the amount of material at the site.

The county road was realigned for approximately 1235 ft. (Exhibit 5.21-1) to accommodate the surface facilities expansion. The road design was performed by Creamer & Noble Engineering. The Applicant designed its runoff control and treatment facility, to control and treat all runoff from the realigned portion of the county road. The design and layout of these structures are discussed in Chapter 7 of this application. Also shown with this information, is a typical design of the county road.

The county will maintain and operate their road, but the Applicant will assume the relocation and reclamation costs during reclamation of the Soldier Canyon Mine. Upon reclamation, the county road will be relocated to its approximate pre-alignment location as shown on Exhibit 5.53-1.

Sewage Lagoons

The ancillary road extending from the county road to the sewage lagoon is an earthen road with two 18" drainage culverts. This road is a remnant of the old county road, once used for travel, up Soldier Canyon. Due to the infrequent use of this road, very little maintenance is performed. The road site ditches and culverts are inspected and maintained as necessary.

Topsoil Storage Site

Access to the topsoil storage site is by an ancillary road extending from the county road. This access road is constructed as shown on Figure 5.34-2 with two 18" drainage culverts. The design of these culverts is discussed in Chapter 7.

To minimize erosion along the road out slopes, riprap was placed on the out slopes. As required by the regulations, culverts will be inspected to ensure that they are functioning as per design.

Refuse Disposal Site

~~The access road, classified as a primary road, will consist of a paved all-weather surface from the county road to the crest of the ephemeral drainage (see Plate 5-1). The road into the drainage will consist of a graveled surface which will be treated to minimize dust and maintenance. The all-weather section of the road will not change, while the gravel portion will have a dynamic location depending on the location of the active refuse disposal are. The designs, specifications, and plans for these roads are presented in Appendix 5-B.~~

~~The stability of the road was also addressed in the EarthFax Engineering, Inc. geotechnical report. As indicated in Appendix 5-A, the road will have a minimum static safety factor of at least 1.3.~~

~~Drainage from the road will be collected in road side ditches and conveyed under the road via drainage culverts. These ditches and culverts are sized to handle the 10 year 6 hour precipitation event. The designs for these structures are discussed in Chapter 7 of this application.~~

~~During the life of the road and disposal facilities, SECC will maintain the access road as necessary to provide adequate access to the site and to prevent environmental damage which might result from the road. To minimize erosion and sediment from the road out slopes, the out slopes of the road will be vegetated with the temporary seed mix as discussed in Section 3.31 of this application.~~

5.35 Spoil

No significant excess spoil will be developed by the underground mine. The only anticipated spoil will be from the materials collected in the sediment pond and during construction of the facilities. This limited volume of material will be removed from the pond and construction site, and transported to the a refuse disposal area.

Therefore, no other plans have been developed to handle other significant volumes of spoil materials.

5.36 Coal Mines Wastes

~~The Applicant will not conduct any mining and reclamation activities within the proposed refuse disposal facility until such time as the plans contained within this application have been reviewed and approved by the Division.~~

~~A general description of the refuse pile construction procedures is presented in Section 5.28 of this chapter. A geotechnical investigation of the refuse pile foundations, conducted by EarthFax Engineering, Inc., indicates an anticipated static safety factor of at least 1.5. The data for this investigation are presented in Appendix 5-A.~~

Refuse disposed of for in the facility will be placed in a controlled manner, as discussed in Section 5.28, and will not result in any impounding of water.

5.37 Regraded Slopes

5.37.10 Geotechnical Analysis

Analyses were performed to determine the stability of cut slopes associated with the Soldier Canyon Mine. The results of these analyses are contained in Appendix 7-E, Part A-3 Slope stability Analysis.

5.37.20 through 5.37.25 Regrading of Fills

At this time, it is Soldier Creek's intention that all fill areas will be regraded to achieve approximate original contour or to achieve a reclaimed surface which blends into the natural contours of the surrounding areas. The contours representing the proposed reclaimed surface are shown on Map 760a.

Refuse Disposal Site

~~As discussed in Section 5.28, once the refuse reaches the design elevation, the refuse material will be regraded to the surface configuration conforming to the proposed topography of the final regraded surface. This proposed surface is indicated on Plate 5-2. The slopes of the final refuse pile will be quite flat (10H:1V) over most of the upper surface of the pile. In the immediate area of the lower portion of the restored drainage channel and along the final face of the refuse pile, the slopes will be 3H:1V. This slope configuration will~~

~~maximize the refuse material storage volume, while maintaining a reclaimable slope. It will also simulate the pediment surface in the surrounding area and the steeper slopes of the incised drainages.~~

~~The cross sections indicated on Plate 5-2 were used to estimate the volumes of topsoil, fill, and refuse. These volume determinations are presented in Appendix 5-C.~~

5.40 Reclamation Plan

5.41 General

5.41.10 through 5.41.40 Permanent Closure of all Facilities

When Soldier Creek Coal Company permanently ceases operation of its Soldier Canyon Mine it will be totally reclaimed in accordance with the R614 Rules and this permit. All underground openings will be sealed and backfilled. All surface equipment, facilities, and structures will be removed, except as described in Section 5.52 below. The proposed postmining land use, and performance standards of the State Program will be achieved through reclamation efforts as described below.

5.42 Narratives, Maps, and Plans

5.42.10 Timetable

A timetable of the final reclamation activities is shown in Table 5.42-1.

5.42.20 through 5.42.32 Final Surface Configuration

Contours representing the final reclaimed surface are shown on Map 760a. Soldier Creek Road will be relocated to its approximate original location and will remain to achieve postmining land use. The main channel of Soldier Creek and the west tributary to Soldier Creek will be reconstructed and will remain after final reclamation. Three culverts will remain to protect the environment after final reclamation. These culverts are described in Section 7.60. All other equipment, structures, and facilities will be removed and reclaimed.

In order to determine the feasibility of achieving the reclaimed surface shown on Map 760 a mass-balance calculations were done. These calculations show that there is more fill material available than is required to achieve the final reclaimed surface. But there is not so much excess material that disposal of the excess material is a problem.

The following procedure was used to calculate the cut and fill material balance for reclamation purposes:

A map showing the projected reclaimed contours was placed over a map showing the disturbed contours. Wherever the contour lines of these two maps intersected points were marked and the differences in the two intersecting contour lines were calculated. If the intersecting contour lines showed that the existing surface had to be cut to achieve the reclamation surface then the difference at the point of intersection was given a positive value to indicate that material would be available. If the contours indicated that the existing surface would have to be raised to meet the reclamation surface then the difference at that intersection point was given a negative value to indicate that fill material would be needed. Cut and fill contours were then drawn for the disturbed areas. The contour lines were drawn on a two foot contour interval except in one area where less detail was needed and a ten foot contour interval was used. The areas between contour lines were then measured using a planimeter. Each area was measured two to four times and the average of the measurements was used. The conversion factor for the planimeter which was used is 1.5254 times the planimeter reading to get the area in square inches. Since maps having a scale of 1 inch equals 50 feet were used the areas in square inches were then multiplied by 2,500 to get the measured area in square feet. The thickness of cut or fill was determined by using the average values of the two thickness contours bounding an area. For example, to determine the thickness of the area measured between the 2 foot and 4 foot contour lines, the average of 3 was calculated. This thickness multiplied by the measured area results in the volume of cut or fill for the area. If an area was bounded by a contour line on the lower limit but not on the upper limit then the thickness was determined by adding one fourth of the contour interval to the value of the bounding contour. For example, if an area was measured within a 10 foot contour line but there was no 12 foot contour line, the thickness assigned to the area bounded by the 10 foot contour was 10.5 feet. This assumption is based on the fact that the area within the 10 foot contour line is greater than 10 feet in thickness but the maximum thickness within this area is less than 12

feet. Areas outside a 0 thickness contour line, or between a 0 cut thickness contour and a 0 fill thickness contour, were assumed to be approximately balanced regarding cut and fill volumes. In these areas there may be an actual net cut or fill amount, but since the differences in the existing surface and the reclamation surface are too small to contour the actual net amounts will be very small with reference to the total volumes involved. As will be discussed below there is excess fill material available so if there is a small deficiency in fill material in these "balanced areas" there is ample fill material available. If these "balanced areas" contain slightly more material than is needed, the additional volume available will not significantly impact the disposition of the excess fill material available from the rest of the project.

The entire disturbed area was measured for cut and fill volumes. The areas of cut and fill are shown on Map 5.42a, Reclamation Volumes. The actual measurements and calculated volumes for each area are shown in Table 5.42-1 below.

TABLE 5.42-1

LOCATION	LINE	READING	ADJUSTMENT	AREA	THICKNES S	VOLUME
Excavate Culvert	+0	31.45	-29.35	8,008	+1	8,008
	+2	25.14	-21.90	12,356	+3	37,067
	+4	21.90	-19.02	10,983	+5	54,914
	+6	19.02	-15.95	11,707	+7	81,952
	+8	15.95	-13.11	10,830	+9	97,473
	+10	13.11	-4.81	31,652	+11	348,173
	+12	4.81	-3.85	3,661	+13	47,592
	+14	3.85	-2.91	3,585	+15	53,770
	+16	2.91	-2.15	2,898	+17	49,270
	+18	2.15	-1.15	3,814	+19	72,457
	+20	1.15	-0.58	2,174	+21	45,648
	+22	0.58	-0.05	2,021	+23	46,487
	+24	0.05	-	191	+24.5	4,672
	+2	1.11	-0.50	2,326	+3	6,979
	+4	0.50	-0.33	3,241	+5	16,207
	+6	0.33	-0.07	992	+7	6,941
	+8	0.07	-0.01	229	+9	2,059
	+10	0.01	-	38	+10.5	418
	+12	3.10	-1.29	6,902	+13	89,732
	+14	1.29	-0.84	1,716	+15	25,741
	+16	0.84	-0.55	1,106	+17	18,801
	+18	0.55	-0.24	1,182	+19	22,462
+20	0.24	-0.05	725	+21	15,216	
+22	0.05	-	191	+22.5	4,290	
Parking Area	+0	6.05	-3.47	9,839	+5	49,194
	+10	3.47	-1.34	8,123	+15	121,841

LOCATION	LINE	READING	ADJUSTMENT	AREA	THICKNES S	VOLUME
	+20	1.34	-	5,110	+22.5	114,977
No.1 Fan	+0	12.28	-9.00	12,508	+1	12,508
	+2	9.00	-1.61	28,182	+3	84,545
	+4	1.61	-0.97	2,441	+5	12,203
	+6	0.97	-0.52	1,716	+7	12,013
	+8	0.52	-	1,983	+8.5	16,856
	+4	0.59	-0.43	610	+5	3,051
	+6	0.43	-0.35	305	+7	2,136
	+8	0.35	-0.31	152	+9	1,373
	+10	0.31	-0.26	191	+11	2,097
	+12	0.26	-0.23	114	+13	1,487
	+14	0.23	-0.15	305	+15	4,276
	+16	0.15	-0.10	191	+17	3,241
	+18	0.10	-0.02	305	+19	5,797
	+20	0.02	-	76	+20.5	1,564
Central Facilities	+0	9.14	-5.00	15,788	+1	15,788
	+2	4.93	-3.60	5,072	+3	15,216
	+4	3.60	-2.82	2,975	+5	14,873
	+6	2.82	-1.94	3,356	+7	23,491
	+8	1.94	-0.89	4,004	+9	36,038
	+10	0.89	-	3,394	+11	37,334
	+12	0.07	-	267	+12.5	3,337
	-0	14.42	-7.98	24,559	-1	-24,559
	-2	7.98	-6.29	6,445	-3	-19,334
	-4	6.29	-4.62	6,369	-5	-31,843
	-6	4.62	-1.73	11,021	-7	-77,147
	-8	1.73	-0.33	5,339	-9	-48,050
	-10	0.33	-	1,258	-10.5	-13,214

LOCATION	LINE	READING	ADJUSTMENT	AREA	THICKNES S	VOLUME
	+0	0.07	-0.03	153	+1	153
	+2	0.03	-	114	+2.5	286
	+0	0.50	-0.05	1,716	+1	1,716
	+2	0.05	-0.01	153	+3	458
	+4	0.01	-	38	+4.5	172
	+0	1.72	-0.91	3,089	+1	3,089
	+2	0.91	-0.56	1,335	+3	4,004
	+4	0.56	-0.23	1,258	+5	6,292
	+6	0.23	-0.07	610	+7	4,271
	+8	0.07	-	267	+8.5	2,269
New Portal Area	-0	16.67	-11.37	20,212	-1	-20,212
	-2	1.44	-1.00	1,678	-3	-5,034
	-4	1.00	-0.46	2,059	-5	-10,296
	-6	0.46	-0.20	992	-7	-6,941
	-8	0.20	-0.09	419	-9	-3,775
	-10	0.09	-	343	-10.5	-3,604
	-2	0.85	-0.29	2,136	-5	-12,813
	-10	0.29	-0.14	572	-11	-6,292
	-12	0.14	-	534	-12.5	-6,674
	-2	9.08	-7.08	7,627	-3	-22,881
	-4	7.08	-5.10	7,551	-5	-37,754
	-6	5.10	-3.38	6,559	-7	-45,915
	-8	3.38	-1.91	5,606	-9	-50,453
	-10	0.12	-	458	-11	-5,034
	-10	1.79	-0.98	3,089	-11	-33,978
	-12	0.98	-0.46	1,983	-13	-25,779
-14	0.46	-0.18	1,068	-15	-16,017	
-16	0.18	-	686	-16.5	-11,326	

LOCATION	LINE	READING	ADJUSTMENT	AREA	THICKNES S	VOLUME
	+0	0.70	-0.16	2,059	+1	2,059
	+2	0.16	-0.07	343	+3	1,030
	+4	0.07	-0.01	229	+5	1,144
	+6	0.01	-	38	+6.5	248
New Facilities	+0	0.70	-0.16	2,059	+1	2,059
	+2	0.16	-0.07	343	+3	1,030
	+4	0.07	-0.01	229	+5	1,144
	+6	0.01	-	38	+6.5	248
	-0	4.37	-3.32	4,004	-1	-4,004
	-2	3.32	-2.35	3,699	-3	-11,097
	-4	2.35	-1.53	3,127	-5	-15,635
	-6	1.53	-1.01	1,983	-7	-13,881
	-8	1.01	-0.47	2,059	-9	-18,531
	-10	0.47	-	1,792	-10.5	-18,816
	-0	22.14	-19.27	10,945	-1	-10,945
	-2	19.27	-16.78	9,496	-3	-28,487
	-4	16.78	-14.64	8,161	-5	-40,804
	-6	14.64	-11.18	13,195	-7	-92,363
	-8	11.18	-9.00	8,313	-9	-74,821
	-10	9.00	-6.91	7,970	-11	-87,672
	-12	6.91	-3.00	14,911	-13	-193,840
	-14	3.00	-1.28	6,559	-15	-98,388
	-16	1.28	-0.30	3,737	-17	-63,533
	-18	0.30	-	1,144	-18.5	-21,165
No.2 Fan Area	+0	8.48	-2.72	21,966	+1	21,966
	+2	2.72	-1.50	4,652	+3	13,957
	+4	1.50	-	5,720	+4.5	25,741
	+0	0.50	-0.10	1,525	+1	1,525

LOCATION	LINE	READING	ADJUSTMENT	AREA	THICKNES S	VOLUME
	+2	0.10	-0.02	305	+3	915
	+4	0.02	-	76	+4.5	343
	-0	0.70	-0.55	572	-1	-572
	-2	0.55	-0.31	915	-3	-2,746
	-4	0.31	-	1,182	-4.5	-5,320
Balanced	0	21.85	-	83,325	0	0
Areas	0	1.71	-	6,521	0	0
	0	12.62	-	48,126	0	0
Subtotal Cut Areas				277,850	Cut Volume	1,847,684
Subtotal Fill Areas				222,027	Fill Volume	1,341,545
Subtotal Balanced Areas				137,972	-	-
Total Area				637,849	Net Volume	506,139

In addition to cut material being used to fill the areas necessary to achieve the reclaimed surface, material will be required to backfill shafts and portals on the property. It was assumed that the material backfilled into the portals will stand at the angle of repose inby the fill. It was also assumed that the shafts will require 10 percent more material than calculated because some of the material will flow into the entries at the bottoms of the shafts. These additional amounts of fill are listed as "Internal Embankments". Table 5.42-2 shows the volume of fill material required to backfill the shafts and portals. Although the proposed 20 foot diameter ventilation shaft is included in the mass balance calculations the costs associated with reclaiming it are not included in this application. The reasons for this are: it is almost certain that the shaft will be constructed and allowance must be made for providing material to backfill it; the cost of reclaiming the new shaft and fan installation will be included in the permit amendment to obtain approval for construction of this facility.

TABLE 5.42-2

PORTALS	NUMBER	WIDTH	HEIGHT	VOLUME OF FILL REQUIRED
	3	20 Feet	16 Feet	15,360
	3	24 Feet	14 Feet	14,112
	2	20 Feet	8 Feet	2,560
SHAFTS	NUMBER	DIAMETER	DEPTH	VOLUME OF FILL REQUIRED
	1	16 Feet	105 Feet	21,112
	1	20 Feet	300 Feet	94,248
Volume Required				147,392
Additional Internal Embankments (30° Angle of Repose)				39,276
Total Volume Required				186,668

Part of the cut/fill volumes determined by the contouring method above consisted of the volume of the large Soldier Creek bypass culvert. The volume of the culvert was measured because it was shown below surface on the disturbed surface contour map and it was removed on the reclaimed surface contour map. The volume of the culvert must be subtracted from the measured volume of material available. The area of the culvert is 239 square feet and it is 893 feet long which results in a volume of 213,427 cubic feet.

The net material available after the disturbed surface has been graded to match the reclamation contours and the culvert volume is subtracted is 292,712 cubic feet. To backfill the portals and shafts requires 186,668 cubic feet which leaves 106,044 cubic feet or 3,928 cubic yards of material. Additionally there are 6,764 cubic yards of topsoil and substitute topsoil located in the topsoil storage area which will also be used to achieve reclaimed contours. This makes the total amount of material which is available but not needed to achieve the reclaimed surface 10,692 cubic yards. The reclamation channel design requires that 6,699 cubic yards of riprap and 3,211 cubic yards of filter gravel be used. This material will replace fill material. This brings the total excess cut material to 20,602 cubic yards. ~~At this time Soldier Creek Coal Company commits to use all excess material to provide a portion of the cover required to be~~

~~placed over the wash plant refuse material. It is estimated that the refuse pile will cover an area of approximately 64 acres. If the excess material from the mine area is spread over 64 acres it will form a cover just over 2.3 inches thick. It is the intention of Soldier Creek Coal Company to contemporaneously reclaim the refuse pile. At final reclamation the only portion of the refuse pile which will not have been reclaimed will be the final face, which is estimated to be 3 acres in size. If, at this time, the excess material from the mine site is spread over the final face of the refuse pile it will provide a cover of fill material slightly in excess of 4 feet in thickness. This will actually enhance the reclamation effort of the refuse pile. Disposal of this material is environmentally feasible.~~

Topsoil is available from several sources. The topsoil storage site contains 2,970 cubic yards of topsoil and 3,794 cubic yards of substitute topsoil. A small topsoil storage pile near the sediment pond contains 310 cubic yards of topsoil. The material under the parking area contains an estimated 3,920 cubic yards of substitute topsoil. The total amount of topsoil and substitute topsoil available is around 10,994 cubic yards or 296,838 cubic feet. The total central mine disturbed area is approximately 14.6 acres. Of this about 10.3 acres are pre-SMCRA. The balance of 4.3 acres, or 187,308 square feet, is post-SMCRA disturbance. Of this 187,308 square feet 32,400 square feet will be paved for the replacement of County Road 53 and 21,400 square feet will be riprapped for reclamation of Soldier Creek. This leaves 133,508 square feet of post-SMCRA area. If 1 foot of topsoil or substitute topsoil is placed on the post-SMCRA area, 133,508 cubic feet of growing media will be required. This leaves 163,330 cubic feet of growing media to place over the pre-SMCRA disturbed area which is around 448,668 square feet in size. The sediment pond is 48,126 square feet in area and 10,595 square feet of stream channel will be riprapped leaving 389,947 square feet to be covered with growing media. The available growing media will provide a cover of just over 5 inches over the pre-SMCRA disturbed area.

While the areas which are assumed to be approximately cut/fill balanced do not contribute to the amount of cut or fill material involved, these areas will be graded to achieve a surface which matches the reclamation contours. The volume of grading associated with each of these areas was determined by measuring the approximate cut area and multiplying the area by the estimated average contour

elevation difference. Reclamation cost calculations include grading costs for the amount of material to be graded and topsoil spreading and seeding costs for the area of each of these locations. The area and grading volume for each area is shown on Map 5.42a.

It is planned that the sediment pond will remain intact during final reclamation to treat disturbed area runoff. The material which was used to construct the sediment pond will be used to totally reclaim the sediment pond area. There is approximately 4500 cubic yards of topsoil and substitute topsoil in the sediment pond embankment. This material will provide a 2.5 foot cover of growing media for reclamation of the sediment pond area. The fact that the sediment pond will be reclaimed some time after the rest of the mine is reclaimed does not affect the final mass-balance calculations or the reclamation cost calculations since the ultimate contoured surface will be achieved regardless of the timing of specific phases of reclamation.

During final backfilling and grading, any fill material, which has been or will be determined to be unsuitable, will be placed at the lowest level against highwalls. Suitable fill material will then be placed over the unsuitable material. The application of topsoil will be as described in chapter 2.00. Otherwise, fill material will be backfilled and graded in the most efficient and effective manner at the time of reclamation in order to achieve reclamation performance standards. The locations of where fill materials are available and where backfilling is required along with the volumes associated with each are shown on Map 5.42a. This map shows where and how much material will be excavated and where and how much material will be backfilled.

Refuse Disposal Site

Reclamation Plan

~~As indicated, no facilities will remain after operations are reclaimed. Upon cessation of operations, due to the phased construction and reclamation of the refuse pile, it is estimated that few facilities will remain to be reclaimed. These facilities will consist of the access road, the active portion of the refuse pile, the sediment pond and associated runoff control structures, and the temporary topsoil storage area.~~

~~The reclamation of the refuse disposal site will consist of site regrading, fill and topsoil placement, reseeding, and soil stabilization. The specific configuration for site regrading are presented as a topographic contour map and cross-sections (see Plate 5-2 and Appendix 5-C). As discussed in Sections 2.40, 5.28 and 5.37, the area will be graded and smoothed to the final topographic configuration. The refuse material will be reworked to break down the large pieces of refuse and then will be compacted by at least three passes of a compactor or other piece of construction equipment with comparable load distribution. The all-weather road surface will be removed and the length of the road area will be ripped to a depth of at least 12 inches. Construction staking will ensure that proper grades are being maintained.~~

~~Following the regrading, the fill and topsoil stored in the temporary topsoil storage area will be distributed according to the plan presented in Section 2.40 of this application. During the placement and distribution of the fill and topsoil, efforts will be made to maintain a uniform thickness over the entire area to be reclaimed.~~

~~Once the soil materials are distributed, the seed bed will be prepared. This will be done in accordance with the topsoil plan presented in Section 2.40 and 2.43 of this application. The seed bed preparation will include scarification and addition of soil nutrients and amendments.~~

~~Reseeding will be conducted in accordance with the revegetation plan presented in Section 3.41 of this application. The reseeding will be conducted in the fall of the year to allow the greatest possibility of revegetation success.~~

~~Following the reseeding, the soils will be stabilized by application of a mulch as described in Sections 2.44 and 3.41.23 of this application. This practice will assist in minimizing the erosion and maximize the potential for revegetation success.~~

~~Reclamation Timetable~~

~~As indicated above, to ensure a good revegetation effort, the reclamation schedule needs to be planned to allow regrading, redistribution of topsoil, and seed bed preparation to be completed to allow seeding in the fall of the year,~~

~~just prior to the first snows. This schedule is presented in Table 3.41-1 and 5.42-1 of this application.~~

~~Following the revegetation efforts, the sediment control structures, consisting of diversions, containment berms, and sediment pond, will remain in place until the revegetated sites have been adequately protected. It is anticipated that the sediment pond will remain in place until at least two years after the last augmented seeding of the reclaimed surface.~~

~~The reclamation of the sediment pond will be accomplished by using the original access road for the observation wells, around the Anderson Reservoir. The topographic configuration of the reclaimed sediment pond area is presented on Plate 5-3. Following reclamation of the sediment pond, the access road will be reclaimed.~~

5.42.40 Bond Release

Before seeking bond release Soldier Creek will provide a description of the structures, which will remain in place. These structures will be maintained, during the reclamation monitoring period, and will be renovated if necessary. Insurance will be provided that all temporary structures will be removed and reclaimed.

5.42.50 Sedimentation Ponds

The sedimentation pond at the Soldier Canyon Mine will remain in place until such time as effluent limitations and vegetative requirements have been met. The sedimentation pond will then be removed and reclaimed. As described above and in Section 7.60, the material used to construct the sedimentation pond will be used to reclaim it to the final contours as shown on Map 760a. The reclaimed sedimentation pond area will then be monitored and maintained for an additional 10 year period.

5.42.60 through 5.42.63 Roads

As part of the 1991 facilities expansion at the Soldier Canyon Mine, Soldier

Creek Road was relocated. Upon final reclamation, the road will be reconstructed in its approximate original location. Culverts, necessary to maintain the integrity of the road, will be permanently installed and will be maintained during the reclamation monitoring period. All other roads in the permit area will be removed and reclaimed. Culverts and bridges associated with the reclaimed roads will be removed. Access to the reclaimed roads will be prevented by the use of large boulders or other type of acceptable barriers.

5.42.70 through 5.42.71 Mine Openings

When no longer needed for mining operations, all entry ways or other openings to the surface from the underground mine will be sealed and backfilled. The permanent closures will be constructed to prevent access to the mine workings by people, livestock, and wildlife. Also, they will keep any potential surface drainage from entering the sealed entries.

Because of the geology of the coal seam, the entries will slope away from the portal pad; therefore, there should be no gravity discharge of water from the underground mine. Furthermore, there are low concentrations of acid producing and no iron producing elements found in any of the coal seams to be mined. The Applicant does not anticipate any discharge from the permanently abandoned mine portals. The analysis of the overburden and underburden indicates an absence of any acid or toxic material.

The abandonment procedures for the portal and shaft openings are in accordance with MSHA procedures (30 CFR 75.1771) and are as follows:

- * Slope or drift openings required to be sealed under 75.1711 shall be sealed with solid, substantial, incombustible material, such as concrete blocks, bricks or tile, or shall be completely filled with incombustible material for a distance of at least 25 feet into such openings.

- * Shaft openings required to be sealed under 75.1711 shall be effectively capped or filled. Filling shall be for the entire depth of the shaft and, for the first 50 feet from the bottom of the coalbed, the fill

shall consist of incombustible material. Caps consisting of a 6-inch thick concrete cap or other equivalent means may be used for sealing. Caps shall be equipped with a vent pipe at least 2 inches in diameter extending for a distance of at least 15 feet above the surface of the shaft.

This procedure for permanent closure of portal entries is shown on Figure 5.42.1. Exposed coal outcrops will be covered with a minimum of 4 ft. of non-combustible earth material to protect against spontaneous combustion. The Applicant will submit detailed design drawings and specifications for sealing the shafts to the Regulatory Authority and MSHA for approval prior to permanent closure of the openings.

5.42.72 through 5.42.74 Disposal of Spoil and Waste

Excess spoil and coal mine waste will be placed in the lowest level of the final fill under cover of unsuitable fill material. This will be done in such a way as to ensure that reclamation performance standards are achieved.

Noncoal mine wastes, ~~when in use~~ will be stored to prevent fires, contamination or other hazards. These wastes will be temporarily disposed of in a metal trash bin until permanently disposed of in an offsite state-approved solid waste disposal facility. During final reclamation, no noncoal mine wastes will be disposed of onsite. All such wastes will be removed from the mine site and disposed of in a state-approved solid waste disposal facility.

5.42.80 Estimate of Reclamation Costs

Reclamation of the Soldier Canyon mine consists of demolition of the existing facilities, site preparation-seeding, and rebuilding the portion of County Road 53 which was relocated.

~~Cost data used in the following calculations are primarily from the Means Heavy Construction Cost Data and Means Site Work Cost Data, 1991 Editions. The reasonableness of these data were verified by comparing to results obtained from the Caterpillar Performance Handbook. For example:~~

~~According to the Caterpillar book a Cat 215B Hydraulic Excavator with a 1 cubic yard bucket will have a 30 second cycle time under severe conditions, with an average operator, and 75 percent job efficiency. A "c" fill factor range indicates that the average bucket load will contain 0.8 cubic yards. Absolute productivity of this machine under the assumed conditions is 96 cubic yards per hour. However, this does not allow for spotting time or move time.~~

~~The Means books list the productivity of a 1 cubic yard excavator as 400 cubic yards per day. This indicates that using the Means data is probably conservative. Certain assumptions and calculations could be made which may result in lower calculated reclamation costs. However, the Means data, based on actual performance, provide calculated costs which have greater assurance of covering the actual costs of reclamation.~~

~~Demolition of Existing Facilities:~~

~~The following costs are taken from the 1991 Means Heavy Construction Cost Data. All costs include equipment, labor, overhead, and profit.~~

~~Fencing, Chain Link, remove only \$1.30/lin. foot
Pipe Removal, 4" steel \$5.60/lin. foot
Pavement Removal, bituminous, 4" to 6" \$5.80/sqr. yard
Concrete Removal, 7" to 24" \$185.00/cu. yard~~

~~Building Demolition, incl. disposal
Steel \$0.19/cu. foot
Concrete \$0.27/cu. foot
Mixture of types, average \$0.20/cu. foot
Small Buildings, wood \$0.21/cu. foot~~

~~Table 5.42-3 lists each structure to be demolished as part of reclamation at the Soldier Creek Mine. This table also indicates the cost of demolition.~~

TABLE 5.42-3

DESCRIPTION	MATERIAL	SIZE	COST/UNIT	AMOUNT
Office	Mixture	132,000 cu. ft.	0.20/cu. ft.	26,400
Warehouse	Mixture	15,950 cu. ft.	0.20/cu. ft.	3,190
Old Shop	Mixture	192,000 cu. ft.	0.20/cu. ft.	38,400
New Shop	Mixture	45,936 cu. ft.	0.20/cu. ft.	9,187
Training Rm.	Mixture	17,748 cu. ft.	0.20/cu. ft.	3,550
Amb. Garage	Mixture	11,600 cu. ft.	0.20/cu. ft.	2,320
Bath House	Mixture	96,000 cu. ft.	0.20/cu. ft.	19,200
Storage Shed	Mixture	32,400 cu. ft.	0.20/cu. ft.	6,480
Security Shack	Wood	512 cu. ft.	0.21/cu. ft.	108
Stoker Bin	Steel	1000 cu. ft.	0.19/cu. ft.	190
Control Bldg.	Mixture	1430 cu. ft.	0.20/cu. ft.	286
8,000 Gal. Tank	Steel	1,070 cu. ft.	0.19/cu. ft.	203
	Concrete	50 cu. yd.	185.00/cu. yd.	9,250
4,000 Gal. Tank	Steel	535 cu. ft.	0.19/cu. ft.	102
	Concrete	34 cu. yd.	185.00/cu. yd.	6,290
1,000 Gal. Tank	Steel	134 cu. ft.	0.19/cu. ft.	26
1500 Gal. Tank	Steel	201 cu. ft.	0.19/cu. ft.	38
	Concrete	3 cu. yd.	185.00/cu. yd.	555
60,000 Gal. Tank	Steel	8,022 cu. ft.	0.19/cu. ft.	1,525
Loadout Bin (2)	Mixture	30,000 cu. ft.	0.20/cu. ft.	6,000
Septic Tank	Steel	9,000 cu. ft.	0.19/cu. ft.	1,710
Fan No.1	Mixture	15,400 cu. ft.	0.20/cu. ft.	3,080
Fan No.2	Mixture	15,300 cu. ft.	0.20/cu. ft.	3,060
Crib Wall	Concrete	120 cu. yd.	185.00/cu. yd.	22,200
Sewage Pipe	4" Steel	10,600 ft.	5.60/lin. ft.	59,360
Substation 1	Concrete	18 cu. yd.	185.00/cu. yd.	3,330
Substation 2	Concrete	30 cu. yd.	185.00/cu. yd.	5,550
Belt Conveyor	Mixture	57,000 cu. ft.	0.20/cu. ft.	11,400
Portals (3)	Concrete	228 cu. yd.	185.00/cu. yd.	42,180
Portals (5)	Concrete	370 cu. yd.	185.00/cu. yd.	68,450

DESCRIPTION	MATERIAL	SIZE	COST/UNIT	AMOUNT
Refuse Bin	Mixture	6,667 cu.ft.	0.20/cu.ft.	1,333
Prep. Plant	Mixture	187,500 cu.ft.	0.20/cu.ft.	37,500
Thickener	Mixture	9,620 cu.ft.	0.20/cu.ft.	1,924
Silos (2)	Concrete	300,000 cu.ft.	0.27/cu.ft.	81,000
Transfer Bldg.	Mixture	12,500 cu.ft.	0.20/cu.ft.	2,500
Culvert Ends	Concrete	2,000 cu.ft.	0.27/cu.ft.	540
Culvert	Steel	53,580 cu.ft.	0.19/cu.ft.	10,180
Ditch	Concrete	1,170 cu.ft.	0.27/cu.ft.	316
Small Culverts	Steel	4,700 cu.ft.	0.19/cu.ft.	893
ROM Conveyor	Mixture	19,000 cu.ft.	0.20/cu.ft.	3,800
Reclaim Conv.	Mixture	11,250 cu.ft.	0.20/cu.ft.	2,250
Spec. Coal Conv.	Mixture	4,500 cu.ft.	0.20/cu.ft.	900
Refuse Conv.	Mixture	810 cu.ft.	0.20/cu.ft.	162
Parking Lot	Asphalt	1865 sq.yd.	5.80/sq.yd.	10,817
Office Park.	Asphalt	716 sq.yd.	5.80/sq.yd.	4,153
Old Yard Road	Asphalt	2,881 sq.yd.	5.80/sq.yd.	16,710
New Yard Road	Asphalt	2,055 sq.yd.	5.80/sq.yd.	11,920
Relocated Road and New Portal Road	Asphalt	4,453 sq.yd.	5.80/sq.yd.	25,830
Fencing	Chain Link	2,000 ft.	1.38/ft.	2,760
Powerline	Wire	2,500 ft.	4.18/ft.	10,450
Subtotal Demolition Cost				\$579,480

~~Grading and Backfilling:~~

~~The following costs were taken from 1991 Means Heavy Construction Cost Data and 1991 Means Site Work Cost Data. All costs include labor, equipment, materials, overhead, and profit.~~

~~Excavating, Dozer, 200 HP, 300' Haul, Common \$4.56/c.y.~~

~~Excavating, Hyd. Excavator, 1 c.y. Bucket \$3.76/c.y.~~

~~Backfilling, 200 HP, FEL, 300' Haul, Common Earth \$1.67/c.y.~~

~~Hauling, 12 c.y. Dump Truck, 4 Mile Round Trip \$4.15/c.y.~~

~~Scarify Topsoil, 200 HP Dozer \$16.75/1000~~

~~Spread Topsoil, 75 HP Dozer & Articulated Loader \$15.50/c.y.~~

~~Seeding, Tractor Spreader \$21.00/1000~~

~~Seed Mix \$296.25/acre~~

~~Silt Fence, Installed \$2.95/l.f.~~

~~Wall, Solid Concrete Block \$7.35/s.f.~~

~~Slab, On Grade, 6", No Finish \$94.00/c.y.~~

~~Seedlings, Planted \$2.00 each~~

~~Mulching \$1,300/acre~~

The topsoil storage site contains 2,970 cubic yards of topsoil, 3,794 cubic yards of substitute topsoil, and 1,337 cubic yards of rock for riprap. The costs in Table 5.42b **the bond** include the cost of hauling these materials from the storage site to the mine site to be used in reclamation. Also 8,573 cubic yards of additional riprap and filter gravel will be hauled in from an outside source. These hauling costs are also included. The storage site contains 590 cubic yards of topsoil to be used to reclaim the storage site. The costs listed in the **table below bond** include the cost of redistributing this topsoil on the storage site.

~~It is assumed in the cost calculations that all silt fences will be replaced five times during the reclamation period.~~

~~Table 5.42-4 lists grading, cutting, filling, topsoiling, and seeding activities and costs associated with reclamation of the Soldier Canyon Mine.~~

TABLE 5.42-4

ACTIVITY	QUANTITY	COST/UNIT	AMOUNT
Central Mine Facility			
Excavate Culvert	42,827 cu.yd.	3.76/cu.yd.	\$161,030
Seal Portals	2,510 sq.ft.	7.35/sq.ft.	18,450
Seal Shaft	3.8 cu.yd.	94.00/cu.yd.	357

ACTIVITY	QUANTITY	COST/UNIT	AMOUNT
Grade Balanced Areas	14,022 cu.yd.	4.56/cu.yd.	63,940
Excavate Cut Areas	25,683 cu.yd.	3.76/cu.yd.	96,560
Backfill Shaft	860 cu.yd.	1.67/cu.yd.	1,436
Backfill Portals	2,215 cu.yd.	1.67/cu.yd.	3,700
Backfill Fill Areas	47,179 cu.yd.	1.67/cu.yd.	78,790
Grade to Reclaim Contour	23,397 cu.yd.	4.56/cu.yd.	106,690
Scarify Subgrade	631,706 sq.ft.	16.75/1000 sq.ft.	10,501
Haul Topsoil From Storage Site to Central Facility	2,970 cu.yd. Topsoil 3,794 cu.yd. Sub. 1,337 cu.yd. Rock	4.15/cu.yd.	33,620
Spread Topsoil	15,500 cu.yd.	15.50/cu.yd.	240,250
Seed Mine Site	631,706 sq.ft.	21.00/1000 sq.ft.	13,266
Plant Seedlings	14.5 acres	2.00 each 15/acre	435
Mulch	14.5 acres	1300.00/acre	18,850
Silt Fence	Phase 1 - 54,925 ft. Phase 2 - 8,775 ft.	2.95/ft.	167,915
Lay Rock Riprap and Filter Gravel	9,910 cu.yd.	27.00/cu.yd.	267,570
Haul in Additional Riprap and Filter Gravel	8,573 cu.yd.	4.15/cu.yd.	35,570
Install Culverts	185 ft.	20.00/ft.	3,700
Seed Mix	14.5 acres	296.25/acre	4,296
Topsoil Storage Site and Sewage Lagoons			
Fill Sewage Lagoons	6,222 cu.yd.	4.56/cu.yd.	28,372
Spread Topsoil - Topsoil Storage Site	590 cu.yd.	15.50/cu.yd.	9,145
Spread Topsoil Sewage Lagoons	890 cu.yd.	15.50/cu.yd.	13,795

ACTIVITY	QUANTITY	COST/UNIT	AMOUNT
Seed Topsoil Storage Site	201,505 sq. ft.	21.00/1000 sq. ft.	4,232
Seed Sewage Lagoons	87,120 sq. ft.	21.00/1000 sq. ft.	1,830
Plant Seedlings	6.6 acre	2.00 ea. 15/acre	198
Mulching	6.6 acre	1,300/acre	8,580
Seed Mix	6.6 acre	296.25/acre	1,957
Scarify Sewage Lagoons & Topsoil Storage Site	288,625	16.75/1000 sq. ft.	4,835
Fence Removal	2,875 ft.	1.30/ft.	3,960
Reconstruct County Road 53			
Sub base	3,600 sq. yd.	0.44/sq. yd.	1,584
Grade subgrade	3,600 sq. yd.	0.12/sq. yd.	432
Asphalt 4"	3,600 sq. yd.	6.35/sq. yd.	22,860
Subtotal Site Preparation and Seeding Cost			\$1,448,81
			0

These costs do not include the cost of reclaiming the proposed No. 3 Ventilation Fan and the associated shaft and access road. A permit amendment will be submitted to obtain approval to install the No. 3 Fan and that amendment will include the cost of reclaiming this specific facility.

Table 5.42-5 below lists the activities and costs associated with the reclamation of the refuse disposal site. It is assumed that as the refuse pile is being filled contemporaneous reclamation will take place. Final reclamation will then consist of reclaiming the final face of the refuse pile and removing and reclaiming the access roads and sediment pond. Under the current reclamation plan reclamation of the mine site will result in 20,602 cubic yards of excess fill material. Table 5.42-5 includes the costs of hauling this material from the mine to the refuse pile and spreading this material over the refuse pile.

TABLE 5.42-5

Activity	Quantity	Cost/Unit	Amount
Primary Access Road			
Remove Asphalt	1,560 sq.yd.	5.00/sq.yd.	7,800
Spread Topsoil	1,800 cu.yd.	15.50/cu.yd.	27,900
Remove Culverts	100 ft.	7.45/ft.	745
Grading	3,600 cu.yd.	4.56/cu.yd.	16,416
Mulch	0.65 acre	1300.00/acre	845
Seed Mix	0.65 acre	296.25/acre	193
Spread Seed	28,314 sq.ft.	21.00/1000 sq.ft.	595
Scarify	28,314 sq.ft.	16.75/1000 sq.ft.	475
Remove Signs/Delineators	6 Signs 44 Posts	7.85 each	393
Secondary Access Road			
Ripping	3,300 cu.yd.	1.60/cu.yd.	5,280
Remove Culverts	185 ft.	7.45/ft.	1,378
Grading	2,400 cu.yd.	4.56/cu.yd.	10,944
Spread Topsoil	5,000 cu.yd.	15.50/cu.yd.	77,500
Mulch	2.1 acre	1300.00/acre	2,730
Seed Mix	2.1 acre	296.25/acre	622
Spread Seed	91,476 sq.ft.	21.00/1000 sq.ft.	1,921
Scarify	91,476 sq.ft.	16.75/1000 sq.ft.	1,533
Remove Signs/Delineators	120	7.85 each	942
Refuse Site Sediment Pond			
Remove Fence	1,350 ft.	1.30/ft.	1,755
Remove Culverts	200 ft.	7.45/ft.	1,490
Backfilling	6,600 cu.yd.	1.67/cu.yd.	11,022
Spread Topsoil	4,650 cu.yd.	15.50/cu.yd.	72,075
Seed Mix	2.0 acre	296.25/acre	593
Spread Seed	87,120 sq.ft.	21.00/1000 sq.ft.	1,830

Activity	Quantity	Cost/Unit	Amount
Mulching	2.0 acre	1300.00/acre	2,600
Scarifying	87,120 sq.ft.	16.75/1000 sq.ft.	1,460
Refuse Disposal Pile			
Grading	2,000 cu.yd.	4.56/cu.yd.	9,120
Spread Topsoil	7,600 cu.yd.	15.50/cu.yd.	117,800
Seed Mix	3.0 acre	296.25/acre	900
Spread Seed	130,600 sq.ft.	21.00/1000 sq.ft.	2,745
Mulching	3.0 acre	1300.00/acre	3,900
Haul Excess Fill From Mine	20,602 cu.yd.	4.15/cu.yd.	85,500
Grade Excess Fill	20,602 cu.yd.	4.56/cu.yd.	93,945
Subtotal			566,717

~~Table 5.42-6 summarizes all of the reclamation costs plus engineering and contingency costs of 10 percent each of the subtotal cost.~~

TABLE 5.42-6

Summary of Reclamation Costs

Demolition Costs	\$579,480
Site Preparation and Seeding Costs	1,440,810
Refuse Site Reclamation	566,717
Mobilization and Demobilization of Equipment	2,000
Subtotal	\$2,597,007
Engineering 10%	259,701
Contingency 10%	259,701
Escalation Rate .77%/year (Rounded)	121,500
Total Reclamation Cost	\$3,237,909

5.50 through 5.51 Sealing of Underground Openings

When any underground opening is no longer needed and is to be abandoned, it will be sealed as described in Section 5.42.70 above.

5.52 through 5.52.20 Permanent Features

At this time it is not anticipated that there will be any constructed depressions or permanent impoundments as part of the final reclamation.

5.53 through 5.53-24 Backfilling and Grading

Backfilling and grading will be done so as to create a reclaimed surface which matches the final reclamation contours shown on Map 760a. This will achieve approximate original contour and will allow the reclaimed surface to blend with the surrounding surfaces. Highwall and depressions will be eliminated as shown on Map 760a. The postmining slope of the reclaimed areas will not exceed the angle of repose as determined by the slope of similar material in place surrounding the reclaimed area. The waste rock site will be graded to a slope which is less than the angle of repose.

Postmining contours as shown on Map 760a were designed giving consideration to stream channel design and runoff control. This will minimize erosion and water pollution.

Spoil will be used to backfill areas where fill is required as shown on Map 5.42a, and will be placed at the lowest level possible and will be covered with material, which will provide a growing media for reclamation vegetation.

When backfilling and grading have been completed, the entire area will be scarified to provide a "toothed roughened" surface on which topsoil will be placed. This will prevent slippage of the topsoil. It is not anticipated that terraces will be used in final reclamation.

~~5.53.25 through 5.53.42 Refuse Piles~~

~~The refuse disposal site will be regraded to provide the final configuration depicted in Plate 5-2. This surface will have a long term static safety factor of at least 1.3 (see Appendix 5-A). Additionally, the surface will minimize erosion and water pollution both on and off site and will support the postmining land use. The surface configuration will consist of a gentle 10H:1V slope across the top of the site, simulating the pediment surface found in the surrounding area, and an incised drainage with 3H:1V sideslopes in the lower part of the restored channel. The face of the refuse pile outslope will also be graded at a 3H:1V slope. This will aid in achieving reclamation success. No cut-and-fill terraces are proposed to be used during the reclamation.~~

~~Based on the chemical characteristics of the proposed refuse material, SECC proposes that the regraded surface be covered with 24-30 inches of fill material and 6-12 inches of topsoil. This fill material will be a nontoxic and noncombustible material. As presented in Chapters 2 and 3 of this application, the feasibility of using this fill depth will be demonstrated through the use of revegetation test plots.~~

~~It is not anticipated that refuse will be stored underground.~~

Exposed coal seams, acid and toxic forming materials, and combustible materials

will be covered with nontoxic and noncombustible materials to prevent combustion or other impact on reclamation.

The use of cut-and-fill terraces is not anticipated in the reclamation of the Soldier Canyon Mine.

5.53.60 through 5.53.65.3 Approximate Original Contour

Much of the disturbance at the Soldier Canyon Mine is pre-SMCRA and information is not available concerning the original contour of these disturbed areas. All areas which have been disturbed post-SMCRA will be reclaimed to the approximate original contour. Pre-SMCRA areas will be returned to the best estimate of approximate original contour and will be contoured to blend in with undisturbed topography adjacent to the disturbed areas. The proposed reclaimed surface of the central mine area is represented by contour lines on Map 760a. No exceptions from these proposed contours are requested.

5.53.70 through 5.53.83 Surface Coal Mining Reclamation Activities

No surface coal mining will be conducted at the Soldier Canyon Mine.

~~5.53.90 Regrading of Settled and Revegetated Pits~~

~~As the refuse disposal site is filled with material from the was plant it will be contemporaneously reclaimed. Any portion of the waste rock site, which is filled to the approximate final contour for that portion will be graded, covered, and vegetated according to R614 and this permit. This will result in most of the surface of the refuse disposal site being completely reclaimed before final reclamation, except for the final face of the pile which will be reclaimed during final reclamation. Since, the reclaimed part of the refuse disposal site will have been graded, settled and vegetated prior to final reclamation, regrading of the reclaimed part of the refuse disposal site during final reclamation will not be required. Only the unreclaimed face of the refuse disposal site will be reclaimed during final reclamation.~~

5.60 Performance Standards

All mining and reclamation operations at the Soldier Canyon Mine will be conducted in accordance with these R614 Rules and this permit.

OFFICE OF SURFACE MINING RECLAMATION AND ENFORCEMENT
BOND AMOUNT COMPUTATION

Applicant Soldier Creek Coal Company

Permit Number ACT/007/018

Date 6 March 1995

Number of Acres 21.82

Type of Operation Underground Coal

Location Soldier Canyon; Carbon County, Utah

Prepared by Gary E. Taylor

Without Surface Expansion

INCORPORATED
EFFECTIVE
OCT 20 1995
G.E.
UTAH DIVISION OF OIL, GAS AND MINING

Project SC³
Date 6 March 1995

WORKSHEET NO. 2
STRUCTURE DEMOLITION AND DISPOSAL COST SUMMARY

Listing of Buildings to be Demolished:

<u>Item</u>	<u>Type of Construction Material</u>	<u>Volume (cubic feet)</u>	<u>Unit Cost Basis</u>	<u>Demolition Cost</u>
1)	See Attached Sheet			
2)				
3)				
4)				
5)				

Total Cost = \$ _____

Other Items to be Demolished:

Debris Handling and Disposal Costs:

TOTAL DEMOLITION AND DISPOSAL COST = \$ 929,758

INCORPORATED
EFFECTIVE:
OCT 20 1995
948
UTAH DIVISION OIL, GAS AND MINING

Data Sources:

Means Construction Cost Data, 1995, Edition 53

TABLE 5.42-3

DESCRIPTION	MATERIAL	SIZE	UNIT	COST/UNIT	AMOUNT
OFFICE FOUNDATIONS DISPOSAL	Mixture Included in Warehouse	132,000	cu. ft.	\$0.23	30,360
WAREHOUSE FOOTINGS WALLS FLOORS DISPOSAL	Mixture	15,950 993 1,852 8,059 251	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.23 \$14.91 \$7.41 \$2.78 \$6.40	3,669 14,806 13,723 22,404 1,606
OLD SHOP FOOTINGS WALLS FLOORS DISPOSAL	Mixture Concrete Concrete Concrete	192,000 766 1,828 6,033 195	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.23 \$14.91 \$7.41 \$2.78 \$6.40	44,160 11,421 13,545 16,772 1,248
NEW SHOP FOOTINGS WALLS FLOORS DISPOSAL	Mixture Concrete Concrete Concrete	45,936 256 674 4,110 105	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.23 \$14.91 \$7.41 \$2.78 \$6.40	10,565 3,817 4,994 11,426 672
TRAINING RM. FOUNDATIONS DISPOSAL	Mixture Included in New Shop	17,748	cu. ft.	\$0.23	4,082
AMB. GARAGE FOUNDATIONS DISPOSAL	Mixture Included in New Shop	11,600	cu. ft.	\$0.23	2,668
BATH HOUSE FOOTINGS WALLS FLOORS DISPOSAL	Mixture Concrete Concrete Concrete	96,000 715 1,590 4,197 153	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.23 \$14.91 \$7.41 \$2.78 \$6.40	22,080 10,661 11,782 11,668 979
STORAGE SHED FOOTINGS WALLS FLOORS DISPOSAL	Mixture Concrete Concrete Concrete	32,400 431 4,906 4,080 261	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.23 \$14.91 \$7.41 \$2.78 \$6.40	7,452 6,426 36,353 11,342 1,670
SECURITY SHACK	Mixture	512	cu. ft.	\$0.23	118
STACKING TUBE FOUNDATIONS DISPOSAL	Steel Concrete	2,500 34 34	cu. ft. cu. yd. cu. yd.	\$0.21 \$95.00 \$6.40	525 3,230 218
CONTROL BLDG.	Mixture	1,430	cu. ft.	\$0.23	329
8,000 GAL TANK FOOTINGS WALLS FLOORS DISPOSAL	Steel Concrete Concrete Concrete	1,070 60 300 200 17	cu. ft. sq. ft. sq. ft. sq. ft. cu. yd.	\$0.21 \$14.91 \$7.41 \$2.78 \$6.40	225 895 2,223 556 109
4,000 GAL TANK FOOTINGS	Steel Concrete	535 60	cu. ft. sq. ft.	\$0.21 \$14.91	112 895

INCORPORATED
 FIGURE 229
 OCT 26 1995
 948
 DIVISION OF ENERGY AND MINING

WALLS	Concrete	300	sq. ft.	\$7.41	2,223
FLOORS	Concrete	200	sq. ft.	\$2.78	556
DISPOSAL		17	cu. yd.	\$6.40	109
1,000 GAL TANK	Steel	134	cu. ft.	\$0.21	28
FOUNDATIONS	Concrete	0	cu. yd.	\$95.00	0
DISPOSAL		0	cu. yd.	\$6.40	0
1,500 GAL TANK	Steel	201	cu. ft.	\$0.21	42
FOUNDATIONS	Concrete	0	cu. yd.	\$95.00	0
DISPOSAL		0	cu. yd.	\$6.40	0
60,000 GAL TANK	Steel	8,022	cu. ft.	\$0.21	1,685
FOUNDATIONS	Concrete	52	cu. yd.	\$95.00	4,940
DISPOSAL		52	cu. yd.	\$6.40	333
LOADOUT BIN	Mixture	15,000	cu. ft.	\$0.23	3,450
FOOTINGS	Concrete	810	sq. ft.	\$14.91	12,077
DISPOSAL		53	cu. yd.	\$6.40	339
SEPTIC TANK	Steel	9,000	cu. ft.	\$0.21	1,890
FAN NO. 1	Mixture	15,400	cu. ft.	\$0.23	3,542
FAN NO. 2	Mixture	15,300	cu. ft.	\$0.23	3,519
CRIB WALL	Concrete	120	cu. yd.	\$212.00	25,440
SEWAGE PIPE	4" Steel	10,600	cu. ft.	\$6.35	67,310
SUBSTATION 1	Concrete	18	cu. yd.	\$212.00	3,816
DISPOSAL		18	cu. yd.	\$6.40	115
SUBSTATION 2	Concrete	30	cu. yd.	\$212.00	6,360
DISPOSAL		30	cu. yd.	\$6.40	192
BELT CONVEYOR	Mixture	57,000	cu. ft.	\$0.23	13,110
FOOTINGS	Concrete	352	sq. ft.	\$14.91	5,248
DISPOSAL		37	cu. yd.	\$6.40	237
PORTALS (3)	Concrete	228	cu. yd.	\$212.00	48,336
PORTALS (5)	Concrete	370	cu. yd.	\$212.00	78,440
CULVERT ENDS	Concrete	74	cu. yd.	\$212.00	15,688
CULVERT	Steel	53,580	cu. ft.	\$0.21	11,252
DITCH	Concrete	43	cu. yd.	\$212.00	9,116
SMALL CULVERTS	Steel	4,700	cu. ft.	\$0.21	987
PARKING LOT	Asphalt	1,865	sq. yd.	\$6.60	12,309
OFFICE PARK	Asphalt	716	sq. yd.	\$6.60	4,726
OLD YARD ROAD	Asphalt	2,881	sq. yd.	\$6.60	19,015
NEW YARD ROAD	Asphalt	2,055	sq. yd.	\$6.60	13,563
RELOCATED ROAD AND NEW PORTAL ROAD	Asphalt	4,453	sq. yd.	\$6.60	29,390
FENCING	Chain Link	2,000	ft.	\$2.29	4,580
POWERLINE	Wire	2,500	ft.	\$4.81	12,025
ON-SITE DISPOSAL		30,563	cu. yd.	\$6.40	195,603
Subtotal Demolition Cost					INCORPORATED \$953,376

OCT 20 1995
948

Project Soldier Creek Coal

Date 25 April 1995

WORKSHEET NO. 5

PRODUCTIVITY AND HOURS REQUIRED FOR DOZER USE

Earthmoving Activity:

Rough Grade

Characterization of Dozer Used (type, size, etc.):

D9N Dozer with "U" Blade - 650 Cy/Hr.

Description of Dozer Use (origin, destination, grade, haul distance, material, etc.):

300 LF + 5% Effective Grade, Material is fill and well blasted.

Productivity Calculations:

$$\begin{aligned} \text{Operating Adjustment Factor} &= \frac{.75}{\text{operator factor}} \times \frac{.80}{\text{material factor}} \times \frac{.83}{\text{work hour factor}} \times \frac{.9}{\text{grade factor}} \times \frac{.94}{\text{weight correction factor}} \times \frac{1.0}{\text{production method/blade factor}} \\ &= \frac{.80}{\text{visibility}} \times \frac{.96}{\text{elevation}} \times \frac{.80}{\text{direct drive transmission}} = .26 \end{aligned}$$

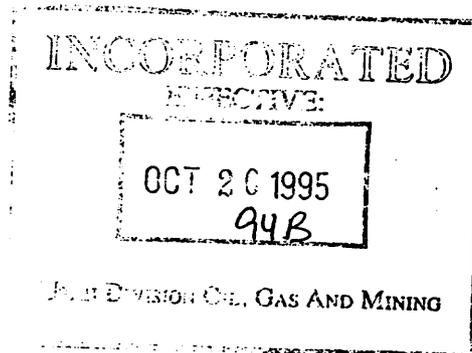
$$\text{Net Hourly Production} = \frac{650 \text{ yd}^3/\text{hr}}{\text{normal hourly production}} \times \frac{.26}{\text{operating adjustment factor}} = 168.25 \text{ yd}^3/\text{hr}$$

$$\text{Hours Required} = \frac{90,820 \text{ yd}^3}{\text{volume to be moved}} \div \frac{168.25 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = 532.82 \text{ hrs}$$

Assume three dozers are required for 179.93 Hr./Ea.

Data Sources:

Caterpillar Performance Handbook; Edition 24



Project Soldier Creek Coal

Date 25 April 1995

WORKSHEET NO. 6

PRODUCTIVITY AND HOURS REQUIRED FOR DOZER USE--GRADING

Earthmoving Activity:

Spread Topsoil

Characterization of Dozer Used (type, size, etc.):

Caterpillar - D4C

Description of Dozer Use (push distance, % grade, blade effective length, operating speed, etc.):

300 L.F. + 5% Effective Grade

Productivity Calculations:

$$\begin{aligned} \text{Operating Adjustment Factor} &= \frac{.75}{\text{operator factor}} \times \frac{1.20}{\text{material factor}} \times \frac{.83}{\text{work hour factor}} \times \frac{.9}{\text{grade factor}} \times \frac{.94}{\text{weight correction factor}} \times \frac{1.0}{\text{production method/blade factor}} \\ &\quad \times \frac{.80}{\text{visibility}} \times \frac{.88}{\text{elevation}} \times \frac{.80}{\text{direct drive transmission}} = \underline{.36} \end{aligned}$$

$$\text{Hourly Production} = \frac{2.2 \text{ mi/hr}}{\text{speed}} \times \frac{15.42}{\text{eff. blade width}} \text{ ft} \times 5280 \text{ ft/mi} \times 1 \text{ ac}/43,560 \text{ ft}^2 = \underline{4.11} \text{ ac/hr}$$

$$\text{Net Hourly Production} = \frac{4.11 \text{ ac/hr}}{\text{hourly prod.}} \times \frac{.36}{\text{op. adj. factor}} = \underline{1.46} \text{ ac/hr}$$

$$\text{Hours Required} = \frac{21.82 \text{ ac}}{1.46 \text{ ac/hr}} = \underline{14.92} \text{ hrs}$$

Data Sources:

Caterpillar Performance Handbook, Edition 21

INCORPORATED

EFFECTIVE:

OCT 20 1995

94B

COAL, GAS AND MINING

Project SC³

Date 6 March 1995

WORKSHEET NO. 8

PRODUCTIVITY AND HOURS REQUIRED FOR LOADER USE

Earthmoving Activity:

Loading Topsoil and Riprap

Characterization of Loader Used (type, size, etc.):

Caterpillar 966 E

Description of Loader Use (origin, destination, grade, haul distance, etc.):

50 LF + 2% Effective Grade

Productivity Calculations:

$$\text{Cycle time} = \frac{.08}{\text{haul time (loaded)}} + \frac{.06}{\text{return time (empty)}} + \frac{.55}{\text{basic cycle time}} = \underline{.69 \text{ min}}$$

$$\text{Net Bucket Capacity} = \frac{5.0 \text{ yd}^3}{\text{heaped bucket capacity}} \times \frac{.95}{\text{bucket fill factor}} = \underline{4.75 \text{ yd}^3}$$

$$\text{Net Hourly Production} = \frac{4.75 \text{ yd}^3}{\text{net/bucket capacity}} \div \frac{.69 \text{ min}}{\text{cycle time}} \times \frac{50 \text{ min/hr}}{\text{work hour factor}} = \underline{344.20 \text{ yd}^3/\text{hr}}$$

$$\text{Hours Required} = \frac{12,241 \text{ yd}^3}{\text{volume to be moved}} \div \frac{344.20 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = \underline{35.56 \text{ hrs}}$$

Data Sources:

Caterpillar Performance Handbook, Edition 21

INCORPORATED
EFFECTIVE:

OCT 20 1995

94B

USE DIVISION OIL, GAS AND MINING

A-109

Project Soldier Creek Coal

Date 25 April 1995

WORKSHEET NO. 8

PRODUCTIVITY AND HOURS REQUIRED FOR LOADER USE

Earthmoving Activity:

Backfill Portals

Characterization of Loader Used (type, size, etc.):

915 Eimco LHD

Description of Loader Use (origin, destination, grade, haul distance, etc.):

250 L.F. 0% Grade

Productivity Calculations:

$$\text{Cycle time} = \frac{1.14}{\text{haul time (loaded)}} + \frac{1.14}{\text{return time (empty)}} + \frac{.41}{\text{basic cycle time}} = \underline{2.71 \text{ min}}$$

$$\text{Net Bucket Capacity} = \frac{6 \text{ yd}^3}{\text{heaped bucket capacity}} \times \frac{.8}{\text{bucket fill factor}} = \underline{4.80 \text{ yd}^3}$$

$$\text{Net Hourly Production} = \frac{4.80 \text{ yd}^3}{\text{net bucket capacity}} \div \frac{2.71 \text{ min}}{\text{cycle time}} \times \frac{50 \text{ min/hr}}{\text{work hour factor}} = \underline{88.56 \text{ yd}^3/\text{hr}}$$

$$\text{Hours Required} = \frac{32,778 \text{ yd}^3}{\text{volume to be moved}} \div \frac{88.56 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = \underline{370.12 \text{ hrs}}$$

Data Sources:

INCORPORATED
EFFECTIVE:

OCT 20 1995

94B

UTAH DIVISION OIL, GAS AND MINING

Project SC³
 Date 6 March 1995

WORKSHEET NO. 9

PRODUCTIVITY AND HOURS REQUIRED FOR TRUCK USE

Earthmoving Activity:

Topsoil and Riprap Hauling

Characterization of Truck Used (type, size, etc.):

12 Yd. Dump Truck

Description of Truck Use (origin, destination, grade, haul distance, truck capacity, etc.):

4 Mile haul one way

Productivity Calculations:

$$\text{Cycle time} = \frac{6.86}{\text{haul time}} + \frac{6.00}{\text{return time}} + \frac{2.53}{\text{total loading time}} + \frac{2.2}{\text{dump and maneuver time}} = 17.59 \text{ min}$$

$$\text{Number of Trucks Required} = \frac{17.59}{\text{truck cycle time}} \div \frac{2.53}{\text{total loading time}} = 6$$

$$\text{Production Rate} = \frac{12 \text{ yd}^3}{\text{truck capacity}} \times \frac{6}{\# \text{ of trucks}} \div \frac{17.59 \text{ min}}{\text{cycle time}} = 4.09 \text{ yd}^3/\text{min}$$

$$\text{Hourly Production} = \frac{4.09 \text{ yd}^3/\text{min}}{\text{production rate}} \times \frac{50 \text{ min/hr}}{\text{work hour factor}} = 204.66 \text{ yd}^3/\text{hr}$$

$$\text{Hours Required} = \frac{18,474 \text{ yd}^3}{\text{volume to be moved}} \div \frac{204.66 \text{ yd}^3/\text{hr}}{\text{hourly production}} = 90.27 \text{ hrs}$$

$$21,120 \text{ ft.} / 3,520 \text{ FPM} = 6.00 \text{ Minutes}$$

$$21,120 \text{ ft.} / 3,080 \text{ FPM} = 6.86 \text{ Minutes}$$

Data Sources:

INCORPORATED

EFFECTIVE:

OCT 20 1995

94B

DEWELON OIL, GAS AND MINING

Project SC³
 Date 6 March 1995

WORKSHEET NO. 9A
 PRODUCTIVITY AND HOURS REQUIRED FOR TRUCK USE

Earthmoving Activity:

Haul Sub-Base

Characterization of Truck Used (type, size, etc.):

20 Ton Bottom Dumps

Description of Truck Use (origin, destination, grade, haul distance, truck capacity, etc.):

Haul Distance - 25 Miles one way

Productivity Calculations:

$$\text{Cycle time} = \frac{33.33}{\text{haul time}} + \frac{30.00}{\text{return time}} + \frac{8}{\text{total loading time}} + \frac{.5}{\text{dump and maneuver time}} = 71.83 \text{ min}$$

$$\text{Number of Trucks Required} = \frac{71.83}{\text{truck cycle time}} \div \frac{8}{\text{total loading time}} = 9$$

$$\text{Production Rate} = \frac{15.59 \text{ yd}^3}{\text{truck capacity}} \times \frac{9}{\# \text{ of trucks}} \div \frac{71.83 \text{ min}}{\text{cycle time}} = 1.95 \text{ yd}^3/\text{min}$$

$$\text{Hourly Production} = \frac{1.95 \text{ yd}^3/\text{min}}{\text{production rate}} \times \frac{60 \text{ min/hr}}{\text{work hour factor}} = 97.67 \text{ yd}^3/\text{hr}$$

$$\text{Hours Required} = \frac{396 \text{ yd}^3}{\text{volume to be moved}} \div \frac{97.67 \text{ yd}^3/\text{hr}}{\text{hourly production}} = 4.05 \text{ hrs}$$

$$\text{Haul } 132,000 \text{ ft.} / 3,960 \text{ ft/mn} = 33.33$$

$$\text{Return } 132,000 \text{ ft.} / 4,400 \text{ ft/mn} = 30.00$$

Data Sources:

INCORPORATED
 EFFECTIVE:
 OCT 20 1995
 94B

DIVISION OIL, GAS AND MINING

Project SC³
Date 6 March 1995

WORKSHEET NO. 10

PRODUCTIVITY FOR HYDRAULIC EXCAVATOR USE (BACKHOE OR POWER SHOVEL)

Earthmoving Activities:

Excavate Culvert

Characterization of the Excavator Used (type, size, etc.):

Caterpillar 215 D LC Excavator

Description of Excavator Used (loading geometry, materials, etc.):

Productivity Calculations:

$$\text{Net bucket capacity} = \frac{1.36 \text{ yd}^3}{\text{heaped bucket capacity}} \times \frac{.70}{\text{fill factor}} = \underline{.95 \text{ yd}^3}$$

$$\text{Net Hourly Production} = \frac{.95 \text{ yd}^3}{\text{net bucket capacity}} \times \frac{55 \text{ min/hr}}{\text{work hour factor}} \div \frac{.33 \text{ min}}{\text{cycle time}} = \underline{158.33 \text{ yd}^3/\text{hr}}$$

$$\text{Hours Required} = \frac{42.827 \text{ yd}^3}{\text{volume to be handled}} \div \frac{158.33 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = \underline{270.49 \text{ hrs}}$$

Data Sources:

Caterpillar Performance Handbook, Edition 21

INCORPORATED
EFFECTIVE

OCT 20 1995

948

UTILITY DIVISION OIL, GAS AND MINING

Project SC³
Date 6 March 1995

WORKSHEET NO. 10 A

PRODUCTIVITY FOR HYDRAULIC EXCAVATOR USE (BACKHOE OR POWER SHOVEL)

Earthmoving Activities:

Excavate Cut Areas

Characterization of the Excavator Used (type, size, etc.):

Caterpillar 215 D LC Excavator

Description of Excavator Used (loading geometry, materials, etc.):

Productivity Calculations:

$$\text{Net bucket capacity} = \frac{1.36 \text{ yd}^3}{\text{heaped bucket capacity}} \times \frac{.70}{\text{fill factor}} = .95 \text{ yd}^3$$

$$\text{Net Hourly Production} = \frac{.95 \text{ yd}^3}{\text{net bucket capacity}} \times \frac{55 \text{ min/hr}}{\text{work hour factor}} \div \frac{.33 \text{ min}}{\text{cycle time}} = 158.33 \text{ yd}^3/\text{hr}$$

$$\text{Hours Required} = \frac{25,683 \text{ yd}^3}{\text{volume to be handled}} \div \frac{158.33 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = 162.21 \text{ hrs}$$

Data Sources:

Caterpillar Performance Handbook, Edition 21

INCORPORATED
RECEIVED:
OCT 20 1995
948
AND MINING

Project SC³
Date 6 March 1995

WORKSHEET NO. 10 B

PRODUCTIVITY FOR HYDRAULIC EXCAVATOR USE (BACKHOE OR POWER SHOVEL)

Earthmoving Activities:

Place Riprap and Filter Blanket

Characterization of the Excavator Used (type, size, etc.):

Caterpillar 215 D LC Excavator

Description of Excavator Used (loading geometry, materials, etc.):

Pick up material and place

Productivity Calculations:

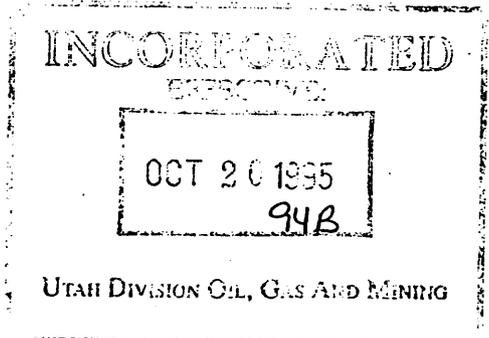
$$\text{Net bucket capacity} = \frac{.36 \text{ yd}^3}{\text{heaped bucket capacity}} \times \frac{.70}{\text{fill factor}} = .95 \text{ yd}^3$$

$$\text{Net Hourly Production} = \frac{.95 \text{ yd}^3}{\text{net bucket capacity}} \times \frac{45 \text{ min/hr}}{\text{work hour factor}} \div \frac{.33 \text{ min}}{\text{cycle time}} = 129.55 \text{ yd}^3/\text{hr}$$

$$\text{Hours Required} = \frac{9,910 \text{ yd}^3}{\text{volume to be handled}} \div \frac{129.55 \text{ yd}^3/\text{hr}}{\text{net hourly production}} = 76.50 \text{ hrs}$$

Data Sources:

Caterpillar Performance Handbook¹, Edition 21



Project SC³
 Date 6 March 1995

WORKSHEET NO. 12

PRODUCTIVITY AND HOURS REQUIRED FOR MOTORGRADER USE--GRADING

Earthmoving Activity:

Grade Sub-Base

Characterization of Grader Used (type, size capacity, etc.):

Caterpillar 14 G

Description of Grader Route (push distance, % grade, blade effective length, operating speed, etc.):

Effective Blade Width - 8 ft.

Speed - 2.4 MPH

Productivity Calculations:

Contour Grading:

$$\text{Hourly Production} = \frac{2.4 \text{ mi/hr} \times 8 \text{ ft}}{\text{speed} \times \text{eff. blade width}} \times 5280 \text{ ft/mi} \times 1 \text{ ac}/43,560 \text{ ft}^2 \times \frac{.3 \text{ work hour factor}}{1} = 0.70 \text{ ac/hr}$$

Scarification:

$$\text{Hourly Production} = \frac{\text{work speed} \times \text{scarifier width}}{\text{work hour factor}} \times 5280 \text{ ft/mi} \times 1 \text{ ac}/43,560 \text{ ft}^2 = \text{ac/hr}$$

$$\text{Hours Required} = \frac{1.49 \text{ ac}}{0.70 \text{ ac/hr}} = 2.13 \text{ hrs}$$

Data Sources:

Caterpillar Performance Handbook, Edition 21

INCORPORATED

ENGINEERING

OCT 20 1995

948

GAS AND MINING

Project Soldier Creek Coal

Date 25 April 1995

WORKSHEET NO. 13

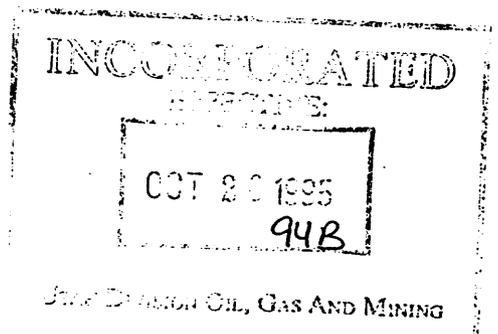
SUMMARY CALCULATION OF EARTHMOVING COSTS

Equipment Type	Owning and Operating Cost (\$/hr) Equipment + Accessories	Labor Cost (\$/hr)	Total Hrs Req'd	Total Cost (\$)
	54,010			
DN9 Dozer (3)	((\$17,610/Machine/Mo. ³)	+ 32.50	1 x 179.93 (3) =	71,553
D4C Dozer	((70.00)	+ 32.50	1 x 14.96 =	1,529
966 E Loader	((46)	+ 32.50	1 x 35.56 =	2,791
915 LHD	((40)	+ 32.50	1 x 370.12 =	26,834
12 Yd Truck 6	((32.50)	+ 22.15	1 x 90.27 =	29,600
20 Ton Truck	((52.00)	+ 22.40	1 x 4.05 =	2,711
	14,813			
215 D Escavator	((\$5,120 Mo. x 2.89 Mo.)	+ 32.50	1 x 509.20 =	31,362
14G Motorgrader	((4,200)	+ 32.50	1 x 2.13 =	169
	(()	+	1 x =	
	(()	+	1 x =	
	(()	+	1 x =	
	(()	+	1 x =	
Total Cost =				<u>166,549</u>

Equipment and Accessory Identification:

Data Sources:

Wheeler Machinery Rental Rates
W.W. Clyde, Equipment and Labor Rental Sheet



Project SC³
Date 6 March 1995

WORKSHEET NO. 14
REVEGETATION COSTS

Name and Description of Area to be Revegetated:

Description of Revegetation Activities:

Reseeding:

$\frac{21.82}{\text{(\# of acres to be reseeded)}} \text{ acres} \times (\$ \frac{\quad}{\text{(\$/acre for seedbed preparation)}} \text{ per acre} + \$ \frac{1,692}{\text{(\$/acre for seeding, fertilizing, and mulching)}} \text{ per acre}) = \$ 36,919$
(costs for reseeded)

Planting Trees and Shrubs:

$\frac{21.82}{\text{(\# of acres for planting)}} \text{ acres} \times \$ \frac{300}{\text{(\$/acre for planting trees and shrubs)}} \text{ per acre} = \$ 6,546$
(costs for planting)

Other Revegetation Activity for this Area (e.g., Soil Sampling):

(Describe and provide cost estimate with documentation; use additional sheets if necessary.)

15 Trees/AC X \$20/Tree = \$300/AC

TOTAL REVEGETATION COST FOR THIS AREA = \$ 43,465

Data Sources:

Means Building Construction Cost Data, Edition 53

INCORPORATED

OCT 20 1995

948

UTAH DIVISION OF OIL, GAS AND MINING

Project SC³
Date March 6, 1995

WORKSHEET NO. 15
OTHER RECLAMATION ACTIVITY COSTS

Descriptions of Reclamation Activity:

Seal Portals
Seal Shaft - 6" Slab on Grade
Silt Fence Installation - 63,700 ft.
Remove Pavement - 4"
Remove Signs/Delineators - 6 Signs, 44 Posts

Assumptions:

Seal Portal - Cost per Block = \$.91 3 Men to complete work in 3 days, 8 Hours/Day
Seal Shaft - Pump Truck = \$17.10/Cu.Yd., Concrete \$75.00/Cu.Yd. = \$92.10
Silt Fence Installed - \$.34/ft., 2 Laborers @ \$17.80/Ea. 800 ft./ Hr. Installation
Remove pavement - \$6.60/sq. yd.
Remove signs/delineators - \$15.65/sign, \$8.95/Delineators

Cost Estimate Calculations:

Remove Signs/Delineators - $\$15.65 \times 6 + \$8.95 \times 44 = \$488$
Seal Portals - $2,510 \text{ sq./ft.} \times \$9.08/50 \text{ ft.} = \$22,800$
Seal Shafts - $3.8 \text{ cu.yd.} \times \$92.10/\text{cu.yd} = 350$
Silt Fence Installation - $63,700 \text{ ft.} \times \$.34/\text{ft.} + \frac{63,700}{800 \text{ pr.hr.}} \times \$17.80 \times 2 = \$24,493$
Remove Pavement - $1,560 \text{ sq. yd.} \times \$6.60 = \$10,296$ TOTAL = \$ _____

Other Documentation or Notes:

(Include additional sheets, maps, calculations, etc., as necessary to document estimate.)

Data Sources:

Means Construction Cost Data 1995, Edition 53

INCORPORATED
SPECIFIC:

OCT 20 1995

948

ENGINEERS AND MINING

Project SC³
Date 6 March 1995

WORKSHEET NO. 15
OTHER RECLAMATION ACTIVITY COSTS

Descriptions of Reclamation Activity:

Asphalt Reconstructed County Road

Assumptions:

10,692 Cu. Ft. x 145 lb./cu.ft. = 1,550,340 lbs. ÷ 2000 lb/ton = 775.17 Ton

Cost Estimate Calculations:

775.17 Tons x \$34.50/Ton = \$26,743

TOTAL = \$ 85,170

Other Documentation or Notes:

(Include additional sheets, maps, calculations, etc., as necessary to document estimate.)

Data Sources:

Means Building Construction Cost Data, Edition 53

INCORPORATED
ENGINEERS

OCT 20 1995
94B

Utah Division Of Gas And Minerals

Project Soldier Creek Coal
Date 25 April 1995

WORKSHEET NO. 16
RECLAMATION BOND SUMMARY SHEET

1. Total Facility and Structure Removal Costs	\$ <u>953,376</u>
2. Total Earthmoving Costs	<u>166,549</u>
3. Total Revegetation Costs	<u>43,465</u>
4. Total Other Reclamation Activities Costs	<u>85,170</u>
5. Subtotal: Total Direct Costs	<u>1,249,560</u>
6. Mobilization and Demobilization (at <u>5</u> % of Item 5) (1% to 5% of Item 5)	<u>62,478</u>
7. Contingencies (at <u>7</u> % of Item 5) (see Table 4)	<u>87,469</u>
8. Engineering Redesign Fee (at <u>6</u> % of Item 5) (see Graph 1)	<u>74,973</u>
9. Contractor Profit and Overhead (at <u>8.8</u> % of Item 5) (see Graph 2)	<u>109,961</u>
10. Reclamation Management Fee (at <u>4.4</u> % of Item 5) (see Graph 3)	<u>54,981</u>
11. GRAND TOTAL BOND AMOUNT (Sum of Items 5 through 10)	\$ <u>1,639,422</u>
12. Escalation @ 2.01/Yr. for 2 years	<u>65,905</u>
	<u>1,705,327</u>

Engineering News Record Cost Index: _____ Date: _____

INCORPORATED
EFFECTIVE

OCT 20 1995

94B

UNIT DIVISION OIL, GAS AND MINING